EFFECTS DUE TO SHEAR FLOW
ON THE DIFFUSIVE-THERMAL INSTABILITY
OF PREMIXED GAS FLAMES

By
Y. KORTSARTS (School of Mathematical Sciences, Tel-Aviv University, Israel),
I. KLIAKHANDLER (School of Mathematical Sciences, Tel-Aviv University, Israel),
L. SHTILMAN (School of Engineering, Tel-Aviv University, Israel),
AND
G. I. SIVASHINSKY (School of Mathematical Sciences, Tel-Aviv University, Israel and The
Levich Institute for Physico-Chemical Hydrodynamics, City College of New York)

Abstract. The diffusively unstable premixed gas flame is shown to be strongly af-
fected by the background shear flow tangent to the flame interface. The pertinent flame-
flow interaction alters both the flame stability limits and the character of its nonlinear
evolution. The shear flow may expand the limits of the flame's diffusive instability si-
multaneously inducing new nonlinear saturation and linear dispersion effects similar to
those occurring in KdV systems.

1. Introduction. Since the classical work of Taylor (1953) it is known that the uni-
directional shear flow may markedly enhance the effective diffusivity of the soluble matter
in the streamwise direction. It is therefore interesting to examine how this fundamental
effect may manifest itself in the intrinsic dynamics of premixed gas flames, which are
known to be highly sensitive to the interplay between thermal and molecular diffusivities
of the system (e.g., Sivashinsky, 1990). To make the pertinent flame-flow interaction
problem as simple as possible it is desirable to find a geometrical situation in which the
undisturbed flame is unaffected by the shear flow. The flow enters the play only when
the flame is disturbed. To meet such a requirement one may, for instance, consider a
planar flame moving through a unidirectional shear flow parallel to the flame interface.
Here the planar flame does not sense the underlying shear flow, which may be rather
complex. However, being disturbed, the flame structure will immediately experience the
impact of Taylor diffusivity, which may markedly influence the character of the flame
evolution. Technically, the system is most tractable when the shear flow is completely

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time-independent in the frame of reference attached to the undisturbed flame. Such a situation occurs, for example, in a premixed flame stabilized on a porous cylindrical burner rotating about its axis of symmetry. Neglecting the density variation, this flame-flow system appears as is shown in Fig. 1. In polar coordinates \((\hat{r}, \varphi)\) the pertinent flow-field \((\hat{v}_r, \hat{v}_\varphi)\) reads:\(^1\)

\[
\hat{v}_r = \hat{Q}/(2\pi \hat{r}), \quad \hat{v}_\varphi = \hat{R}_0 \hat{\Omega} / \hat{r}.
\]

Here \(\hat{R}_0\), \(\hat{\Omega}\), and \(\hat{Q}\) are the porous burner radius, the burner rotation rate, and the total flow intensity, correspondingly.

The flow-field (1.1) obviously may sustain a steady cylindrical flame whose interface is located at

\[
\hat{r} = \hat{R} = \hat{Q}/(2\pi \hat{U}_b)
\]

where \(\hat{U}_b\) is the burning velocity of the planar flame. The burner rotation clearly does not affect the circular equilibrium (1.2). Yet, it induces the shear

\[
\frac{d\hat{v}_\varphi(\hat{R})}{d\hat{r}} = -\frac{\hat{R}_0^2 \hat{\Omega}}{\hat{R}^2} = -\hat{\alpha},
\]

which, as will be shown below, may significantly alter the flame stability.

\(^1\)The subscript \(^*\) labels the dimensional quantities.
2. Mathematical model. The stability of the cylindrical (circular) flame (Fig. 1) will be studied within the framework of a conventional constant-density near-equidiffusion model with suitably chosen nondimensional variables and parameters that reads (e.g., Matkowsky and Sivashinsky, 1979)

\[
\frac{\partial \Theta}{\partial t} + v_r \frac{\partial \Theta}{\partial r} + v_\varphi \frac{\partial \Theta}{\partial \varphi} = \frac{\partial^2 \Theta}{\partial r^2} + \frac{1}{r} \frac{\partial \Theta}{\partial r} + \frac{1}{r^2} \frac{\partial^2 \Theta}{\partial \varphi^2},
\]

\[
\frac{\partial S}{\partial t} + v_r \frac{\partial S}{\partial r} + v_\varphi \frac{\partial S}{\partial \varphi} = \frac{\partial^2 (S - \alpha \Theta)}{\partial r^2} + \frac{1}{r} \frac{\partial (S - \alpha \Theta)}{\partial r} + \frac{1}{r^2} \frac{\partial^2 (S - \alpha \Theta)}{\partial \varphi^2}.
\]

Here

\[v_r = \frac{R}{r}, \quad v_\varphi = \frac{aR^2}{r}\]

where \(R = R/\ell_{th}\) is the nondimensional circular flame radius; \(\ell_{th} = \hat{D}_{th}/\hat{U}_b\) where \(\hat{D}_{th}\) is the thermal diffusivity of the system; \(R_0 = R_0/\ell_{th}\); \(a = \hat{\alpha}_{th}/\hat{U}_b\) is the nondimensional shear (1.3);

\[\Theta = \frac{\hat{T} - \hat{T}_0}{\hat{U}_b - \hat{T}_0}\]

is the reduced temperature of the system; \(\hat{T}_0\) is the initial temperature of the fresh mixture; \(\hat{T}_b\) is the adiabatic temperature of the burned gas;

\[S = \frac{(\hat{T}_b - \hat{T}_0)\hat{C} + (\hat{T} - \hat{T}_b)\hat{T}_a}{2\hat{C}_0\hat{T}_b^2}\]

is the reduced enthalpy, where \(\hat{C}\) is the mass fraction of the deficient reactant; \(\hat{C}_0\) is the initial level of mass fraction; \(\hat{T}_a\) is the activation temperature of the chemical reaction \((\hat{T}_a \gg \hat{T}_b)\); \(r = \hat{r}/\ell_{th}\), \(t = \hat{t}\ell_{th}/\ell_{th}\), \(\alpha = \hat{T}_a(\hat{T}_b - \hat{T}_0)(Le^{-1} - 1)/(2\hat{T}_b^2)\), where \(Le = \hat{D}_{th}/\hat{D}_{mol}\) is the Lewis number (the ratio of thermal diffusivity to molecular diffusivity of the deficient reactant). The reaction zone is localized at the interface \(r = \Phi(\varphi, t)\) where the following matching conditions hold:

\[\left[\frac{d\Theta}{dn}\right] + \exp S = 0, \quad (2.4)\]

\[\left[\frac{dS}{dn}\right] = \alpha \left[\frac{d\Theta}{dn}\right], \quad (2.5)\]

\[\Theta = 0, \quad [S] = 0. \quad (2.6)\]

Here

\[n = \frac{(1, -\Phi_\varphi/\Phi)}{\sqrt{1 + (\Phi_\varphi/\Phi)^2}}\]

is an outer normal to the flame interface \(r = \Phi(\varphi, t)\).

In the burned gas, i.e., at \(r > \Phi(\varphi, t)\),

\[\Theta(r, \varphi, t) = 1. \quad (2.7)\]

The model (2.1)–(2.7) is a consistent asymptotics that may be formally derived from a pertinent reaction-diffusion-advection set of equations, provided \(\hat{T}_a \gg \hat{T}_b\) (i.e., the activation temperature is high) and simultaneously \(\alpha \sim (\hat{T}_a/\hat{T}_b)(Le^{-1} - 1)\) is a finite
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parameter (i.e., when $\hat{D}_{th} \simeq \hat{D}_{mol}$). At the entrance of the burner the temperature of
the fresh mixture is $T_0$ and the mass fraction of the deficient reactant is $\hat{C}_0$. Assuming
that there is no heat-mass interaction between the burner skeleton and the flow, one may
set

$$v_r \Theta = \frac{\partial \Theta}{\partial r}, \quad v_r S = \frac{\partial (S - \alpha \Theta)}{\partial r} \quad \text{at} \quad r = R_0. \quad (2.8)$$

For a steady cylindrical flame, i.e., when $\Phi = R$, the problem (2.1)-(2.8) yields the
following basic solution:

$$\Theta^b = \left( \frac{r}{R} \right)^R \quad \text{at} \quad r < R \quad \text{and} \quad \Theta^b = 1 \quad \text{at} \quad r > R, \quad (2.9)$$

$$S^b = \alpha R \left( \frac{r}{R} \right)^R \ln \left( \frac{r}{R} \right) \quad \text{at} \quad r < R \quad \text{and} \quad S^b = 0 \quad \text{at} \quad r > R. \quad (2.10)$$

3. Asymptotic analysis. The nonlinear stability analysis will be carried out near
$\alpha = 1$, the stability threshold of a freely propagating planar flame. Henceforth, $\varepsilon = \alpha - 1$
will be employed as a parameter of expansion. In the absence of rotation, $\Omega = 0$, the
related problem was discussed in Sivashinsky (1979). As has been shown in that study, in
order to have a well-behaved asymptotics at $\varepsilon \to 0$ all the major variables and parameters
of the system should be scaled as follows:

$$\Theta - \Theta^b = \varepsilon^2 \hat{\Theta}, \quad S - S^b = \varepsilon^2 \hat{S}, \quad \Phi - R = \varepsilon \hat{\Phi}, \quad \varphi = \varepsilon^{3/2} \hat{\varphi},$$

$$t = \varepsilon^{-2} \hat{t}, \quad R = \varepsilon^{-2} \hat{R}, \quad R_0 = \varepsilon^{-2} \hat{R}_0, \quad \alpha = 1 + \varepsilon. \quad (3.1)$$

As a result for the leading-order $\varepsilon$-approximation the following flame interface evolution
equation was obtained:

$$\frac{\partial \hat{\Phi}}{\partial \hat{t}} + \frac{1}{2} \left( \frac{\partial \hat{\Phi}}{\partial \hat{x}} \right)^2 + \frac{\partial^2 \hat{\Phi}}{\partial \hat{x}^2} + 4 \frac{\partial^4 \hat{\Phi}}{\partial \hat{x}^4} + \frac{\hat{\Phi}}{\hat{R}} = 0 \quad (\hat{x} = \hat{R} \hat{\varphi}). \quad (3.2)$$

In the problem involving rotation, apart from the time scale associated with the in-
stability induced growth rate, there emerges the second time scale conditioned by the
drift of the large-scale disturbances. To avoid the cumbersome multiple-time asymptotic
expansion it is helpful to pass from the original angular coordinate $\varphi$ to the shifted one

$$\theta = \varphi - at \quad (a = \Omega R^2_0 / R^2) \quad (3.3)$$

where $\theta$ should be scaled as $\varphi$, i.e.,

$$\theta = \varepsilon^{3/2} \hat{\theta}. \quad (3.4)$$

2We mean here the instability leading to the formation of the so-called cellular flames occurring in
low Lewis number premixtures. For high Lewis number systems one may well encounter a different,
pulsating mode of instability. Despite rather scanty experimental data on the phenomenon in gaseous
premixtures, in the combustion of some condensed mixtures, where $Le = \infty$, the pulsating instability
appears to be quite feasible and received a good deal of attention both experimentally and theoretically
(e.g., Bayliss and Matkowsky, 1990).
Apart from the drift the flame interface is also subject to the action of the shear (see (2.3))

\[ \frac{dv_\varphi(R)}{dr} = -a \]  

(3.5)

which is expected to augment the effective diffusivity of the system by a quantity of order \((dv_\varphi/dr)^2\), as happens in Taylor's problem. To make this impact comparable to that of negative diffusivity (see Eq. (3.2)) one should set

\[ (dv_\varphi(R)/dr)^2 \sim \alpha - 1 = \varepsilon. \]  

(3.6)

Hence, the shear should be scaled as

\[ a = \varepsilon^{1/2} \bar{a}. \]  

(3.7)

Rescaling the original problem (2.1)–(2.8) according to (3.1), (3.3), (3.4), (3.7) after a lengthy but otherwise straightforward algebra (see Appendix) one obtains

\[ \frac{\partial \Phi}{\partial \bar{t}} + \frac{1}{2} \left( \frac{\partial \Phi}{\partial \bar{x}} \right)^2 - 2\bar{a} \Phi \frac{\partial \Phi}{\partial \bar{x}} + (1 + 40\bar{a}^2) \frac{\partial^2 \Phi}{\partial \bar{x}^2} - 20\bar{a} \frac{\partial^3 \Phi}{\partial \bar{x}^3} + 4 \frac{\partial^4 \Phi}{\partial \bar{x}^4} + \frac{\Phi}{\bar{R}} = 0 \]  

(\bar{x} = \bar{R}\theta).

(3.8)

As is readily seen from the term \((1 + 40\bar{a}^2)\Phi_{\bar{x}\bar{x}}\), the shear flow promotes the diffusive flame instability.3 One should remember, however, that Eq. (3.8) is an approximation whose range of validity is restricted to the vicinity of \(\alpha = 1\), the stability threshold of a freely propagating planar flame. Equation (3.2) and therefore Eq. (3.8) are not applicable for high Lewis number systems (\(Le > 1, \alpha < 0\)), where the shear flow is likely to exert an opposite, i.e., stabilizing influence. This issue, however, is out of the scope of this study and will be addressed in a future work.

Apart from affecting the stability threshold, the shear flame may generate travelling waves controlled by the dispersive term, \(20\bar{a}\Phi_{\bar{x}\bar{x}}\). The shear also produces a new quadratic nonlinearity \(2\bar{a}\Phi \Phi_{\bar{x}}\), which emerges in numerous extended systems and, on par with the geometric term \(\frac{1}{2}(\Phi_{\bar{x}})^2\), is known to provide the nonlinear saturation of linearly unstable modes (e.g., Michelson and Sivashinsky, 1980). At \(\bar{a} \ll 1\) the geometric nonlinearity clearly dominates over the shear one. However, at \(\bar{a} \gg 1\), since \(\bar{a} \bar{x} \sim 1\), both nonlinearities have a balanced impact on the system; none of them can be ignored. In the latter limit, Eq. (3.8) becomes

\[ \Psi_{\tau} + \frac{1}{2} (\Psi_\xi)^2 - 2\Psi \Psi_\xi + 40\Psi_\xi \xi - 20\Psi_\xi \xi \xi + 4 \Psi_\xi \xi \xi \xi + \gamma^{-1} \Psi = 0 \]  

(3.9)

where

\[ \Psi = \bar{a}^{-2} \Phi, \quad \xi = \bar{a} \bar{x}, \quad \tau = \bar{a}^4 \bar{t}, \quad \gamma = \bar{a}^4 \bar{R}. \]

3For example, a low Lewis number stable cylindrical flame may be destabilized by rotation of the burner.
The dispersion relation associated with Eq. (3.9) reads

$$\omega = (40k^2 - 4k^4) - \gamma^{-1} - 20ik^3 \quad (\Psi \sim \exp(\omega t + ik\xi)).$$  \hspace{1cm} (3.10)

The instability sets in at $\gamma > \gamma_c = 1/100$ and $k_c = \sqrt{5}$, the wave number corresponding to the maximum growth rate of small harmonic perturbations.

4. Numerical simulations. In this section we present results of the numerical simulations of Eq. (3.9). The equation was solved over the interval $0 < \xi < 10\lambda_c$ subject to periodic boundary conditions ($\lambda_c = 2\pi k_c^{-1}$). The pseudo-spectral technique has been employed for the spatial discretization and the Adams’ scheme for time advance. Since Eq. (3.9) has a strong damping in the high $k$ range, all the scales were resolved at the

![Figure 2a](image-url)
resolution 512, while the control runs were conducted at the resolution 1024. The calculations were performed on an ALPHA-DEC workstation. As initial data in all simulations, the random fields were used. The problem was solved for three cases: $\gamma_1 = 1.1\gamma_c$, slightly above the stability threshold; $\gamma_2 = 1.33\gamma_c$, close to $\gamma_c$; $\gamma_3 = 5\gamma_c$, significantly above $\gamma_c$.

The spatio-temporal evolution of the flame interface $\Psi$ is plotted in Figs. 2a, 2b, and 2c.

At $\gamma = \gamma_1$ the function $\Psi$ appears to be nearly periodic both in $\xi$ and $\tau$. At $\gamma = \gamma_2$ the regular pattern disappears and at $\gamma = \gamma_3$ the interface dynamics assumes a clearly expressed chaotic behaviour. Yet, the solution still preserves the typical length-scale $\lambda_c$ provided by the linear theory.

With the passage from $\gamma_1$ to $\gamma_3$ the spatial average $\langle \Psi \rangle$ markedly decreases. As a result the emerging corrugated structure undergoes a permanent drift along the $\xi$-axis stemming from the terms $2\Psi\Psi_\xi$ and $20\Psi_{\xi\xi\xi}$ of Eq. (3.9). For the sake of better visualization the interface evolution is shown in a moving frame $\xi' = \xi - V(\gamma)\tau$ with $V(\gamma) \approx 20k_c^2 - 2\langle \Psi \rangle$. 

Fig. 2b. Numerical simulation of Eq. (3.9). $\langle \Psi \rangle$ versus time $\tau$ and $\xi' = \xi - v(\gamma)\tau$ for various values of $\gamma$ ($0 < \xi' < 10\lambda_c$). $\gamma_1 = 1.33\gamma_c$, $v(\gamma_1) = 177.5$, $253 < \tau/\tau_c < 269$, $\tau_c = 2\pi\omega^{-1}(\gamma_2, k_c) = 0.253$. 

\[\begin{array}{c}
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\text{The spatio-temporal evolution of the flame interface } \Psi \text{ is plotted in Figs. 2a, 2b, and } 2c. \\
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\end{array}\]
5. Concluding remarks. The results obtained show that apart from small-scale high-intensity eddies certain slowly-varying fields may also affect the relaxational features of the large-scale flames. It is curious that the found shift in the effective dissipation rate cannot be captured within the framework of the stretch-based geometrical model (e.g., Williams, 1985):

\[ F_t + v \cdot \nabla F = v_F |\nabla F|, \]  
\[ v_F = 1 + (1 - \alpha)(\text{div} \, n + n \cdot \nabla v \cdot n) \]  

Equations (5.1)–(5.2) are written in nondimensional form employing the same set of units as the reaction-diffusion model of Sec. 2. \( F(x, y, z, t) = 0 \) is the flame interface and \( n = -\nabla F/|\nabla F| \) is its normal vector; \( v_F \) is the flame speed relative to the prescribed flow-field \( v \); \( v_F \) depends both on curvature of the flame and on \( v \).
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Appendix A. Formal derivation of Equation (3.8). To conduct the necessary asymptotic expansions it is technically advantageous to perform the following change of spatial variables:

$$\varphi = \theta + at, \quad r = z + \Phi(\theta, t),$$  \hspace{1cm} (A.1)

which eliminates the drift-induced time scale and fixes the location of the reaction zone at $z = 0$. In the new coordinates $(\theta, z, t)$ the set of original equations (2.1)-(2.2) becomes

$$D(\Theta) = L(\Theta), \quad D(S) = L(S - \alpha \Theta)$$  \hspace{1cm} (A.2)

where

$$D = \frac{\partial}{\partial t} + \left[ a\Phi_\theta - \Phi_t + \frac{R}{z + \Phi} - \frac{aR^2\Phi_\theta}{(z + \Phi)^2} \right] \frac{\partial}{\partial z} + \left[ \frac{aR^2}{(z + \Phi)^2} - a \right] \frac{\partial}{\partial \theta},$$  \hspace{1cm} (A.3)

$$L = \left[ 1 + \frac{\Phi_\theta}{(z + \Phi)^2} \right] \frac{\partial^2}{\partial z^2} + \left[ \frac{1}{z + \Phi} - \frac{\Phi_\theta}{(z + \Phi)^2} \right] \frac{\partial}{\partial z} + \frac{1}{(z + \Phi)^2} \frac{\partial^2}{\partial \theta^2} - \frac{2\Phi_\theta}{(z + \Phi)^2} \frac{\partial^2}{\partial z \partial \theta}. $$  \hspace{1cm} (A.4)

The matching conditions (2.4)-(2.6) at the flame interface $z = 0$ become

$$[\Theta] = [S] = 0, \quad \left( \sqrt{1 + \Phi_\theta^2/\Phi^2} \right) [\Theta] + \exp S = 0, \quad [S_2 - \alpha S] = 0.$$  \hspace{1cm} (A.5)

In the burnt gas region

$$\Theta = 1 \text{ at } z > 0 \quad \text{and} \quad S_z \text{ is bounded at } z \rightarrow \infty.$$  \hspace{1cm} (A.6)

At the burner wall where $z = R_0 - \Phi(\theta, t)$, the boundary condition (2.8) yields

$$\Theta_z = R\Theta/R_0, \quad S_z - \alpha \Theta_z = aR^2S/R_0.$$  \hspace{1cm} (A.7)

The basic solution (2.9)-(2.10) corresponding to the undisturbed flame becomes

$$\Theta^b(z < 0) = (1 + (z/R))^R, \quad S^b(z < 0) = aR(1 + (z/R))^R \ln(1 + (z/R)).$$  \hspace{1cm} (A.8)

As the next step one should pass to the scaled quantities as defined by the relations (3.1), (3.2), (3.4), (3.7). In the scaled variables and parameters the problem (A.2)-(A.7) may be written as

$$-\varepsilon^3 \Phi_\theta \Theta_z^b + \varepsilon^2 \Theta_z^b - \varepsilon^3 \Phi \Phi_z^{b-1} \Theta_z^b - 2\varepsilon^3 aR^{-1} z\Theta_\theta^b + 2\varepsilon^2 aR^{-1} z\Phi_\theta \Theta_z^b + 2\varepsilon^3 aR^{-1} z\Phi_\theta \Theta_z^b + \Theta_z^b - \varepsilon^2 z\Theta_z^b$$

$$+ 2\varepsilon^3 aR^{-1} \Phi \Phi_\theta \Theta_z^b + \Theta_z^b - \varepsilon^2 z\Theta_z^b$$

$$= \Theta_z^b + \varepsilon^2 R^{-1} \Theta_z^b + \varepsilon^2 \Theta_{zz}^b + \varepsilon^3 R^{-2} \Theta_{\theta\theta}^b - \varepsilon^2 R^{-2} \Phi_\theta \Theta_z^b + \varepsilon^3 R^{-2} \Phi_\theta \Theta_{zz}^b + O(\varepsilon^4),$$  \hspace{1cm} (A.9)
\[-\varepsilon^3 \Phi_0 S_z^b + \varepsilon^2 S_z - \varepsilon^3 \Phi R^{-1} S_z^b - 2\varepsilon^3 aR^{-1} zS_\theta + 2\varepsilon^2 aR^{-1} z\Phi_\theta S_z^b + 2\varepsilon^3 aR^{-1} \Phi \Phi_\theta^t S_z^b + S_z^b - \varepsilon^2 zS_z^b \]

\[= (S^b - \alpha \Theta^b)_{zz} + \varepsilon^2 R^{-1} (S^b - \alpha \Theta^b)_{z} + \varepsilon^2 (S - \alpha \Theta)_{zz} + \varepsilon^3 R^{-2} (S - \alpha \Theta)_{z} + 0(\varepsilon^4), \tag{A.10} \]

\[[\Theta] = [S] = 0, \quad [S_z - \alpha \Theta] = 0, \quad [\Theta_z] + S - \frac{1}{2} \varepsilon R^{-2} (\Phi_\theta)^2 + 0(\varepsilon^2) = 0 \text{ at } z = 0, \tag{A.11} \]

\[\Theta \to 0, \quad S \to 0 \text{ at } z \to -\infty. \tag{A.12} \]

\[\Theta = 0 \text{ for } z > 0 \text{ and } S \text{ grows not faster than an integer power of } z \text{ at } z \to +\infty. \tag{A.13} \]

The last requirement ensures the compatibility with the boundary condition (A.6) which, unlike (A.7), is achieved not at \( z = O(1) \) but rather at \( z = O(1/\varepsilon) \). Note that the basic solution \( \Theta^b, S^b \) is \( \varepsilon \)-dependent both through \( R = \varepsilon^{-2} R \) and \( \alpha = 1 + \varepsilon \):

\[\Theta^b = \Theta_0^b + O(\varepsilon^2) \text{ where } \Theta_0^b (z < 0) = \exp z \quad \text{and} \quad \Theta_0^b (z > 0) = 1, \tag{A.14} \]

\[S^b = S_0^b + \varepsilon S_1^b + O(\varepsilon^2), \]

where

\[S_0^b (z < 0) = S_1^b (z < 0) = z \exp z, \tag{A.15} \]

and

\[S_0^b (z > 0) = S_1^b (z > 0) = 0. \tag{A.16} \]

The unknown functions \( \Phi, \Theta, \) and \( S \) are sought as asymptotic expansions in integer powers of \( \varepsilon \):

\[\Phi = \Phi^0 + \varepsilon \Phi^1 + O(\varepsilon^2), \quad \Theta = \Theta^0 + \varepsilon \Theta^1 + O(\varepsilon^2), \quad S = S^0 + \varepsilon S^1 + O(\varepsilon^2). \tag{A.17} \]

For the zeroth approximation the system (A.10)–(A.13) yields

\[\Theta_{zz}^0 - S_{zz}^0 = -2aR^{-1} z\Phi_0^0 S_0^b - R^{-2} \Phi_{\theta \theta}^0 \Theta_{0z}^b, \tag{A.18} \]

\[\Theta_{zz}^0 - S_{zz}^0 + \Theta_{zz}^0 = -2aR^{-1} z\Phi_0^0 S_0^b - R^{-2} \Phi_{\theta \theta}^0 S_{0z}^0 + R^{-2} \Phi_{\theta \theta}^0 \Theta_{0z}^b, \tag{A.19} \]

\[\Theta^0 = 0, \quad S^0 \to 0 \quad \text{at} \quad z \to -\infty, \tag{A.20} \]

\[\Theta^0 = 0 \text{ at } z > 0 \quad \text{and} \quad S_z^0 < \infty \text{ at } z \to +\infty. \tag{A.21} \]
Hence, one obtains $\bar{\Theta}^0$, $\bar{S}^0$ expressed in terms of $\Phi^0$ (still unknown at this stage). The solution of the problem (A.17)–(A.18) is of the form

$$\bar{\Theta}^0 (z < 0) = (R^{-2} \Phi^0_{\bar{\theta}\bar{\theta}} - 2aR^{-1} \Phi^0_\theta) z \exp z + aR^{-1} \Phi^0_\theta z^2 \exp z,$$

$$\bar{\Theta}^0 (z > 0) = 0,$$

$$\bar{S}^0 (z < 0) = (R^{-2} \Phi^0_{\bar{\theta}\bar{\theta}} - 2aR^{-1} \Phi^0_\theta) z \exp z + (R^{-2} \Phi^0_{\bar{\theta}\bar{\theta}} - aR^{-1} \Phi^0_\theta) z^2 \exp z$$

$$+ aR^{-1} \Phi^0_\theta z^3 \exp z,$$

$$\bar{S}^0 (z > 0) = R^{-2} \Phi^0_{\bar{\theta}\bar{\theta}} - 2aR^{-1} \Phi^0_\theta.$$ (A.23)

For the first approximation the system (A.10)–(A.13) gives

$$\bar{\Theta}^1_z - \bar{\Theta}^1_{zz} = \Phi^0_t \Theta^0_z + \Phi^0 R^{-1} \Theta^0_{oz} + 2aR^{-1} z\Theta^0_{\bar{\theta}z} - 2aR^{-1} z\Phi^0_\theta \Theta^0_{oz}$$

$$- 2aR^{-1} \Phi^0_\theta \Theta^0_{oz} + R^{-2} \Theta^0_{\bar{\theta}z} - \Phi^0_{\bar{\theta}z} - R^{-2} \Theta^0_{oz} + R^{-2} (\Phi^0_\theta)^2 \Theta^0_{oz},$$ (A.24)

$$\bar{S}^1_z - \bar{S}^1_{zz} + \bar{\Theta}^1_z + \Theta^0_{zz} = \Phi^0_t S^0_z + \Phi^0 R^{-1} S^0_{oz} + 2aR^{-1} zS^0_{\bar{\theta}z} - 2aR^{-1} z\Phi^0_\theta S^0_{oz}$$

$$- 2aR^{-1} \Phi^0_\theta S^0_{oz} + R^{-2} (S^0 - \Theta^0)_{\bar{\theta}z} - \Phi^0_{\bar{\theta}z} R^{-2} (S^0 - \Theta^0)_{oz}$$

$$- \Phi^0_\theta R^{-2} (S^0 - \Theta^0)_{oz} + R^{-2} (\Phi^0_\theta)^2 (S^0 - \Theta^0)_{zz},$$ (A.25)

$$[\bar{\Theta}^1] = [\bar{S}^1] = 0 \text{ at } z = 0,$$ (A.26)

$$[\bar{\Theta}^1_z] + \bar{S}^1_z = \frac{1}{2} R^{-2} (\Phi^0_\theta)^2 \text{ at } z = 0,$$ (A.27)

$$[\bar{\Theta}^1_z - \bar{S}^1_z] = -[\Theta^0_z] \text{ at } z = 0,$$ (A.28)

$$\bar{\Theta}^1 \to 0, \bar{S}^1 \to 0 \text{ at } z \to -\infty,$$ (A.29)

$$\bar{\Theta}^1 = 0 \text{ at } z > 0 \text{ and } \bar{S}^1_{zz} < \infty \text{ at } z \to +\infty.$$ (A.30)

Solution of the system (A.24), (A.25) meeting the conditions (A.26), (A.29), (A.30) and thereby apart from $\Phi^0$, $\Phi^1$ involving also $\bar{S}^1(0)$ reads

$$\bar{\Theta}^1 (z < 0) = (-\Phi^0_t + R^{-4} \Phi^0_{\bar{\theta}\bar{\theta}\bar{\theta}} - 8aR^{-3} \Phi^0_{\bar{\theta}\bar{\theta}} - R^{-2} (\Phi^0_\theta)^2)$$

$$+ 20a^2 R^{-2} \Phi^0_{\bar{\theta}z} + R^{-2} \Phi^0_{zz} - R^{-1} \Phi^0 + 2aR^{-1} \Phi^0_\theta - 2aR^{-1} \Phi^0_\theta z \exp z$$

$$+ (-\frac{1}{2} R^{-4} \Phi^0_{\bar{\theta}\bar{\theta}\bar{\theta}} + 4aR^{-3} \Phi^0_{\bar{\theta}z} - 10a^2 R^{-2} \Phi^0_{\bar{\theta}z} + aR^{-1} \Phi^0_\theta) z^2 \exp z$$

$$+ (-\frac{1}{2} aR^{-3} \Phi^0_{\bar{\theta}z} + \frac{10}{3} a^2 R^{-2} \Phi^0_{\bar{\theta}z}) z^3 \exp z - \frac{1}{2} a^2 R^{-2} \Phi^0_{\bar{\theta}z} z^4 \exp z,$$

$$\bar{\Theta}^1 (z < 0) = 0,$$ (A.31)
\[ S^1(z < 0) = S^1(0) \exp z + (-\Phi_t^0 - 3R^{-1}\Phi_{\theta\theta\theta\theta}^0 + 20aR^{-3}\Phi_{\theta\theta\theta\theta}^0 - R^{-2}(\Phi_\theta^0)^2 \]
\[-4aR^{-2}\Phi_{\theta\theta}^0 - R^{-1}\Phi_t - 3aR^{-1}\Phi_{\theta\theta\theta}^0 - 2aR^{-1}\Phi_{\theta\theta\theta}^0 \exp z + (-\Phi_t^0 + \frac{3}{2}aR^{-4}\Phi_{\theta\theta\theta\theta}^0 - 13aR^{-3}\Phi_{\theta\theta\theta\theta}^0 - R^{-2}(\Phi_\theta^0)^2 + R^{-2}\Phi_{\theta\theta}^0 + 32a^2R^{-2}\Phi_{\theta\theta}^0 + R^{-2}\Phi_{\theta\theta}^0 - R^{-1}\Phi_{\theta\theta}\]
\[-aR^{-1}\Phi_{\theta}^0 + 2aR^{-1}\Phi_{\theta\theta}^0 - aR^{-1}\Phi_{\theta\theta}\exp z + (-\frac{1}{2}R^{-4}\Phi_{\theta\theta\theta\theta}^0 + 4aR^{-3}\Phi_{\theta\theta\theta\theta}^0 - 10a^2R^{-2}\Phi_{\theta\theta\theta}^0 + aR^{-1}\Phi_{\theta\theta\theta}^0 + aR^{-1}\Phi_{\theta\theta}\exp z + (-aR^{-3}\Phi_{\theta\theta}\]
\[+\frac{17}{6}a^2R^{-2}\Phi_{\theta\theta}\exp z + \frac{1}{2}a^2R^{-2}\Phi_{\theta\theta}\exp z^2 \exp z, \]
\[S^1(z > 0) = S^1(0) + (R^{-4}\Phi_{\theta\theta\theta\theta}^0 - 4a^2R^{-2}\Phi_{\theta\theta\theta}^0)\exp z + (\Phi_t^0 - \Phi_{\theta\theta\theta\theta}^0 - 2a^2R^{-2}\Phi_{\theta\theta}\exp z^2. \]

\[(A.32)\]

The remaining boundary conditions (A.27), (A.28) imply
\[ R^{-2}\Phi_{\theta\theta} - 2aR^{-1}\Phi_{\theta} - S^1(0) = \Phi_t^0 + R^{-1}\Phi_t - 20aR^{-2}\Phi_{\theta\theta}^0 + 8aR^{-3}\Phi_{\theta\theta\theta\theta}^0 \]
\[-R^{-4}\Phi_{\theta\theta\theta\theta}^0 - 2aR^{-1}\Phi_{\theta\theta}^0 + \frac{1}{2}R^{-2}(\Phi_\theta^0)^2, \]

\[(A.33)\]

\[ R^{-2}\Phi_{\theta\theta}^0 - 2aR^{-1}\Phi_{\theta} - S^1(0) \]
\[= -2aR^{-1}\Phi_t + R^{-2}(1 + 60a^2)\Phi_{\theta\theta}^0 + 28aR^{-3}\Phi_{\theta\theta\theta\theta}^0 + 5R^{-4}\Phi_{\theta\theta\theta\theta\theta\theta}. \]

\[(A.34)\]

Since the r.h.s. of the relations obtained are identical, they are compatible only provided that their l.h.s. are identical as well. Hence, one ends up with the sought-for equation for the interface \( \Phi_t \):
\[ \Phi_t^0 - 2aR^{-1}\Phi_t^0 + \frac{1}{2}R^{-2}(\Phi_\theta^0)^2 - 2aR^{-1}\Phi_t^0 + R^{-2}(1 + 40a^2)\Phi_{\theta\theta}^0 \]
\[-20aR^{-3}\Phi_{\theta\theta\theta\theta}^0 + 4R^{-4}\Phi_{\theta\theta\theta\theta\theta\theta}^0 + R^{-1}\Phi_\theta^0 = 0. \]

\[(A.35)\]

By a shift transformation \( \bar{\theta} + 2aR^{-1}\bar{t} \to \hat{\theta} \) one eliminates the drift term \(-2aR^{-1}\Phi_t^0\). Setting \( \bar{R}\theta = \bar{x} \) one finally arrives at Eq. (3.8).

REFERENCES