

A TRANSPORT THEOREM FOR MOVING INTERFACES*

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1. The theorem. When studying surface effects within the framework of continuum mechanics one is often confronted with terms of the form

$$\frac{d}{dt} \int_{\mathcal{S}(t)} f(\mathbf{x}, t) da(\mathbf{x}), \quad (1)$$

where $\mathcal{S}(t)$ is a surface which evolves with time t , $f(\mathbf{x}, t)$, defined for all $\mathbf{x} \in \mathcal{S}(t)$ and all t , is the density (per unit area) of a superficial quantity such as energy, and $da(\mathbf{x})$ is the area measure on surfaces in \mathbb{R}^3 . The evaluation of (1) is nontrivial when $\mathcal{S}(t)$ evolves within a fixed region $\Omega \subset \mathbb{R}^3$ and $\partial\mathcal{S}(t) \subset \partial\Omega$ is nonempty, for then a portion of (1) must balance an outflow of f due to the transport of portions of $\mathcal{S}(t)$ across $\partial\Omega$.

We assume that $\mathcal{S}(t)$ is smooth and oriented by $\mathbf{n}(\mathbf{x}, t)$, a particular choice of continuous unit-normal field, and we write $V(\mathbf{x}, t)$ and $\kappa(\mathbf{x}, t)$ for the **normal velocity** and **total curvature**. (Total curvature is twice the normal curvature.) It is the purpose of this note to prove the **transport theorem**:¹

$$\begin{aligned} \frac{d}{dt} \int_{\mathcal{S}(t)} f da &= \int_{\mathcal{S}(t)} (f^\circ - f\kappa V) da - \text{outflow}(f, \partial\mathcal{S}(t)), \\ \text{outflow}(f, \partial\mathcal{S}(t)) &= \int_{\partial\mathcal{S}(t)} f V p (1 - p^2)^{-1/2} ds, \quad p = \mathbf{n} \cdot \boldsymbol{\nu}. \end{aligned} \quad (2)$$

Here f° is the normal time derivative of f as defined below, ds is the measure of length on curves in \mathbb{R}^3 , and $\boldsymbol{\nu}(\mathbf{x})$ is the outward unit normal on $\partial\Omega$.

2. Assumptions and preliminary definitions. It is convenient to identify \mathbb{R}^4 with $\mathbb{R}^3 \times \mathbb{R}$.

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¹An argument in support of (2) is contained in the work Moeckel [1]. Moeckel assumes that the interface can be identified with a "fictitious" (sic) evolving membrane whose boundary coincides with the boundary of the interface at each time, and then appeals to a standard transport theorem for membranes. Unfortunately, Moeckel expresses the outflow in terms of the *membrane* velocity, which is not intrinsic, and which obscures the influence of the confining region Ω . Moreover, the existence of such an evolving membrane is not at all obvious, and, in fact, seems to constitute a mathematical problem more difficult than the original problem of verifying (2). Angenent and Gurtin [2] establish (2) for an evolving curve in a two-dimensional space, but their proof does not extend.

We assume that $\Omega \subset \mathbb{R}^3$ is a bounded, open region with smooth boundary $\partial\Omega$, and write $\nu(\mathbf{x})$ for the outward unit normal on $\partial\Omega$. We assume that $\mathcal{S}(t) \subset \mathbb{R}^3$ is defined for all t in an open interval T and: (S1) $\mathcal{S}(t)$ is the intersection with Ω of a smooth, nonintersecting, oriented surface, and $\partial\mathcal{S}(t) \subset \partial\Omega$; (S2) $\mathbf{n}(\mathbf{x}, t)$, the unit normal to $\mathcal{S}(t)$, satisfies $|\mathbf{n}(\mathbf{x}, t) \cdot \nu(\mathbf{x})| \neq 1$ on $\partial\mathcal{S}(t)$; (S3) the set

$$\mathcal{S}_T = \{(\mathbf{x}, t): \mathbf{x} \in \mathcal{S}(t), t \in T\}$$

is a smooth three-dimensional surface in \mathbb{R}^4 with normal never parallel to the time direction.

We assume that $f(\mathbf{x}, t)$ is a smooth scalar field on \mathcal{S}_T .

We write $\mathbf{N}(\mathbf{x}, t)$ and $\mathbf{U}(\mathbf{x})$, respectively, for $\mathbf{n}(\mathbf{x}, t)$ and $\nu(\mathbf{x})$ considered as unit vectors in \mathbb{R}^4 , and \mathbf{E} for the unit vector in \mathbb{R}^4 in the time direction:

$$\mathbf{N} = (\mathbf{n}, 0), \quad \mathbf{U} = (\nu, 0), \quad \mathbf{E} = (\mathbf{0}, 1). \quad (3)$$

By (S3) there is a scalar field V such that $\mathbf{N} - V\mathbf{E}$ is normal to \mathcal{S}_T ; the field V represents the **normal velocity** of the surface in the direction \mathbf{n} . We write \mathbf{M} for the unit vector in the direction of $\mathbf{N} - V\mathbf{E}$:

$$\mathbf{M} = q(\mathbf{N} - V\mathbf{E}), \quad q = (1 + V^2)^{-1/2}. \quad (4)$$

Then $\mathbf{M}(\mathbf{x}, t)^\perp$ is the tangent plane to \mathcal{S}_T at (\mathbf{x}, t) . We write \mathbf{E}^* for the normalized projection of \mathbf{E} onto \mathbf{M}^\perp :

$$\mathbf{E}^* = q(V\mathbf{N} + \mathbf{E}). \quad (5)$$

Given any field Φ on \mathcal{S}_T , we write $\nabla\Phi$ for the surface gradient² of Φ in \mathcal{S}_T : $\nabla\Phi(\mathbf{x}, t)$ is a vector in $\mathbf{M}(\mathbf{x}, t)^\perp$ if Φ is scalar-valued; it is a linear transformation from $\mathbf{M}(\mathbf{x}, t)^\perp$ into \mathbb{R}^4 if Φ is vector-valued. For Φ a scalar field, we define the **normal time derivative** Φ° through

$$\Phi^\circ = \nabla\Phi \cdot (V\mathbf{N} + \mathbf{E}). \quad (6)$$

We write div for the surface divergence on \mathcal{S}_T : if Φ is a vector field on \mathcal{S}_T , $\text{div}\Phi = \text{trace}[\mathbf{P}\nabla\Phi]$, where $\mathbf{P}(\mathbf{x}, t)$ is the projection of \mathbb{R}^4 onto $\mathbf{M}(\mathbf{x}, t)^\perp$. It is not difficult to verify that

$$\kappa = -\text{div}\mathbf{N} \quad (7)$$

is the **total curvature** of $\mathcal{S}(t)$.

The identity

$$\text{div}\mathbf{E}^* = -q\kappa V \quad (8)$$

is useful. Its verification is not difficult: since $\nabla q = -q^3 V \nabla V$ and $q - q^3 V^2 = q^3$, (5) and (7) yield

$$\text{div}\mathbf{E}^* = qV \text{div}\mathbf{N} + q^3 \nabla V \cdot \mathbf{N} - q^3 V \nabla V \cdot \mathbf{E} = -qV\kappa + q^3 \nabla V \cdot (\mathbf{N} - V\mathbf{E})$$

which implies (8), since $\mathbf{N} - V\mathbf{E}$ is normal to \mathcal{S}_T (cf. (4)).

²Many of the definitions and identities that we use concerning surfaces can be found in [3, 4].

3. Proof of the transport theorem. Given a time interval $R = [t_0, t_1] \subset T$, the surface divergence theorem applied to the vector field $f\mathbf{E}^*$ on

$$\mathcal{S}_R = \{(\mathbf{x}, t) : \mathbf{x} \in \mathcal{S}(t), t \in R\}$$

has the form

$$\int_{\partial \cdot \mathcal{J}_R} f\mathbf{E}^* \cdot \mathbf{W} dA_2 = \int_{\mathcal{J}_R} \operatorname{div}(f\mathbf{E}^*) dA_3. \tag{9}$$

Here dA_n ($n = 1, 2, 3$) is the ‘‘area’’ measure on n -dimensional surfaces in \mathbb{R}^4 , while \mathbf{W} is the outward unit normal to $\partial \mathcal{S}_R$. $\partial \mathcal{S}_R$ is the union of the sets

$$\operatorname{top}(\mathcal{S}_R) = \{(\mathbf{x}, t_1) : \mathbf{x} \in \mathcal{S}(t_1)\},$$

$$\operatorname{bot}(\mathcal{S}_R) = \{(\mathbf{x}, t_0) : \mathbf{x} \in \mathcal{S}(t_0)\},$$

$$\operatorname{side}(\mathcal{S}_R) = \{(\mathbf{x}, t) : \mathbf{x} \in \partial \mathcal{S}(t), t \in T\},$$

whose intersection has zero A_1 -measure, and, trivially,

$$\mathbf{E}^* \cdot \mathbf{W} = 1 \quad \text{on } \operatorname{top}(\mathcal{S}_R), \quad \mathbf{E}^* \cdot \mathbf{W} = -1 \quad \text{on } \operatorname{bot}(\mathcal{S}_R). \tag{10}$$

The computation of $\mathbf{E}^* \cdot \mathbf{W}$ on $\operatorname{side}(\mathcal{S}_R)$ is not so simple. Since

$$p = \mathbf{n} \cdot \boldsymbol{\nu} = \mathbf{N} \cdot \mathbf{U}, \tag{11}$$

(4) and (5) yield

$$\mathbf{U} \cdot \mathbf{M} = qp, \quad \mathbf{U} \cdot \mathbf{E}^* = qpV. \tag{12}$$

If $\mathbf{A} = \mathbf{U} - (\mathbf{U} \cdot \mathbf{M})\mathbf{M}$, the projection of \mathbf{U} onto \mathbf{M}^\perp , then $\mathbf{W} = \mathbf{A}/|\mathbf{A}|$ on $\operatorname{side}(\mathcal{S}_R)$. Thus, using (12),

$$\mathbf{W} = (1 - q^2p^2)^{-1/2}(\mathbf{U} - qp\mathbf{M}) \quad \text{on } \operatorname{side}(\mathcal{S}_R), \tag{13}$$

and, since $\mathbf{M} \cdot \mathbf{E}^* = 0$ and

$$(1 - q^2p^2) = (1 - p^2 + V^2)/(1 + V^2), \tag{14}$$

a simple calculation using (12) leads to

$$\mathbf{E}^* \cdot \mathbf{W} = Vp(1 - p^2 + V^2)^{-1/2} \quad \text{on } \operatorname{side}(\mathcal{S}_R). \tag{15}$$

By (5), (6), and (8), $\operatorname{div}(f\mathbf{E}^*) = q(-fV\kappa + f^\circ)$; thus (9) yields

$$\begin{aligned} & \int_{\operatorname{top}(\mathcal{J}_R)} f dA_2 - \int_{\operatorname{bot}(\mathcal{J}_R)} f dA_2 + \int_{\operatorname{side}(\mathcal{J}_R)} f Vp(1 - p^2 + V^2)^{-1/2} dA_2 \\ &= \int_{\mathcal{J}_R} q(f^\circ - f\kappa V) dA_3. \end{aligned} \tag{16}$$

Further,

$$\int_{\operatorname{top}(\mathcal{J}_R)} f dA_2 = \int_{\mathcal{J}'(t_1)} f da, \quad \int_{\operatorname{bot}(\mathcal{J}_R)} f dA_2 = \int_{\mathcal{J}'(t_0)} f da. \tag{17}$$

The final step is to rewrite the remaining terms in (16) as iterated integrals. For any function g on \mathcal{S}_R ,

$$\int_{\mathcal{J}_R} g dA_3 = \int_{t_0}^{t_1} \left\{ \int_{\mathcal{J}'(t)} g(\mathbf{E}^* \cdot \mathbf{E})^{-1} da \right\} dt = \int_{t_0}^{t_1} \left\{ \int_{\mathcal{J}'(t)} gq^{-1} da \right\} dt, \tag{18}$$

where we have used (5). On the other hand,

$$\int_{\text{side}(\partial\mathcal{S}_R)} g dA_2 = \int_{t_0}^{t_1} \left\{ \int_{\partial\mathcal{S}(t)} g(\mathbf{B} \cdot \mathbf{E})^{-1} ds \right\} dt, \tag{19}$$

where $\mathbf{B}(\mathbf{x}, t)$ with $\mathbf{B} \cdot \mathbf{E} > 0$ is that unit vector in the tangent plane to $\text{side}(\partial\mathcal{S}_R)$ which is normal to $\partial\mathcal{S}(t)$. In fact, $\mathbf{B} = \mathbf{C}/|\mathbf{C}|$, where \mathbf{C} is the projection of \mathbf{E}^* onto \mathbf{W}^\perp :

$$\mathbf{C} = \mathbf{E}^* - (\mathbf{E}^* \cdot \mathbf{W})\mathbf{W}.$$

By (4)₂ and (15),

$$|\mathbf{C}|^2 = q^{-2}(1 - p^2)/(1 - p^2 + V^2).$$

Further, since $\mathbf{E}^* \cdot \mathbf{M} = \mathbf{U} \cdot \mathbf{E} = 0$, (4), (5), (12), and (13) yield

$$\mathbf{E}^* \cdot \mathbf{E} = q, \quad \mathbf{E}^* \cdot \mathbf{W} = q p V(1 - q^2 p^2)^{-1/2}, \quad \mathbf{E} \cdot \mathbf{W} = q^2 p V(1 - q^2 p^2)^{-1/2},$$

and hence, using (14),

$$\mathbf{B} \cdot \mathbf{E} = (1 - p^2)^{1/2}(1 - p^2 + V^2)^{-1/2}.$$

Thus (19) yields

$$\int_{\text{side}(\partial\mathcal{S}_R)} g dA_2 = \int_{t_0}^{t_1} \left\{ \int_{\partial\mathcal{S}(t)} g \{(1 - p^2 + V^2)/(1 - p^2)\}^{1/2} ds \right\} dt. \tag{20}$$

Finally, in view of (17), (18), and (20), (16) reduces to

$$\begin{aligned} & \int_{\mathcal{S}(t_1)} f da - \int_{\mathcal{S}(t_0)} f da + \int_{t_0}^{t_1} \left\{ \int_{\partial\mathcal{S}(t)} f V p / (1 - p^2)^{1/2} ds \right\} dt \\ & = \int_{t_0}^{t_1} \left\{ \int_{\mathcal{S}(t)} (f^\circ - f \kappa V) da \right\} dt; \end{aligned}$$

and differentiation with respect to t_1 yields (2).

REMARK 1. $\mathcal{S}(t)$ is the intersection with Ω of an oriented surface $\mathcal{M}(t)$; let $\boldsymbol{\mu}(\mathbf{x}, t)$, a tangent vector to $\mathcal{M}(t)$ at $\mathbf{x} \in \mathcal{M}(t)$, denote the outward unit normal to $\partial\mathcal{S}(t)$ as a curve in $\mathcal{M}(t)$. The calculation of the outflow term in (2) is essentially the calculation of the velocity $\sigma(\mathbf{x}, t)$ of $\partial\mathcal{S}(t)$ in the direction $\boldsymbol{\mu}(\mathbf{x}, t)$. In fact, if we consider an arbitrary (smoothly-evolving) patch $\mathcal{S}(t)$ of an evolving surface $\mathcal{M}(t)$, then

$$\frac{d}{dt} \int_{\mathcal{S}(t)} f da = \int_{\mathcal{S}(t)} (f^\circ - f \kappa V) da + \int_{\partial\mathcal{S}(t)} f \sigma ds. \tag{21}$$

REMARK 2. It is important to identify the term $\text{outflow}(f, \partial\mathcal{S}(t))$ in (2) as a term representing an outflow of $f(\mathbf{x}, t)$ due to the transport of portions of $\mathcal{S}(t)$ across $\partial\Omega$. If one writes, for example, balance of energy for a continuous body Ω consisting of two phases separated by an interface $\mathcal{S}(t)$ with interfacial energy f , then a term of the form $\text{outflow}(f, \partial\mathcal{S}(t))$ should appear (cf. Gurtin [4]). Moeckel [1] fails to include such an outflow in his balance laws. Fernandez-Diaz and Williams [5] point this out, but unfortunately the outflow term they propose is incorrect, as it does not include the scale factor $(1 - p^2)^{-1/2}$.

REMARK 3. It is possible to write the transport identity (2) in terms of a nonnormal velocity. Indeed, for $\mathbf{v} = V\mathbf{n} + \mathbf{u}$ with $\mathbf{u} \cdot \mathbf{n} = 0$,

$$\frac{d}{dt} \int_{\mathcal{S}'(t)} f da = \int_{\mathcal{S}'(t)} (f^\circ + f \operatorname{div} \mathbf{u}) da - \operatorname{outflow}(f, \partial \mathcal{S}'(t)) \quad (22)$$

where $f^\circ = \nabla f \cdot (\mathbf{v} + \mathbf{E})$ is the derivative following \mathbf{v} , div is the surface divergence on $\mathcal{S}'(t)$, and

$$\operatorname{outflow}(f, \partial \mathcal{S}'(t)) = \int_{\partial \mathcal{S}'(t)} f [Vp(1-p^2)^{-1/2} + \mathbf{u} \cdot \boldsymbol{\nu} (1+p^2)^{-1/2}] ds, \quad p = \mathbf{n} \cdot \boldsymbol{\nu}. \quad (23)$$

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