The Faber Polynomials for Circular Sectors

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Abstract. The Faber polynomials for a region of the complex plane, which are of interest as a basis for polynomial approximation of analytic functions, are determined by a conformal mapping of the complement of that region to the complement of the unit disc. We derive this conformal mapping for a circular sector $\{z: |z| \leq 1, |\arg z| \leq \pi/\alpha\}$, where $\alpha > 1$, and obtain a recurrence relation for the coefficients of its Laurent expansion about the point at infinity. We discuss the computation of the coefficients of the Faber polynomials of degree 1 to 15, which are tabulated here for sectors of half-angle $5^\circ, 10^\circ, 15^\circ, 30^\circ, 45^\circ$, and 90° , and we give explicit expressions, in terms of α , for the polynomials of degree ≤ 3 . The norms of Faber polynomials are tabulated and are compared with those of the Chebyshev polynomials for the same regions.

1. Introduction. In recent years there has been a growing awareness of the potential usefulness of the Faber polynomials as a basis for polynomial and rational approximations in the complex plane. It has been shown [4], [3] that, under mild conditions, a truncated Faber series is a near-minimax polynomial approximation for an analytic function, on the region to which it applies. However, practical exploitation of this result has been hampered by a lack of knowledge of Faber polynomials, except for a few specific regions. In particular, for circular sectors, which provide a convenient subdivision of the plane, the Faber polynomials were hitherto unknown.

For any closed bounded continuum D in the complex plane there is a function ϕ , such that

$$(1) \quad \lim_{z \rightarrow \infty} \frac{\phi(z)}{z} = 1,$$

which maps the complement of D in the extended z -plane conformally onto $\{w: |w| > \rho\}$, the complement of a closed disc of radius ρ (see, e.g., Markushevich [10, v. 3, p. 104]). The number ρ is called the transfinite diameter of D . The function ϕ has a Laurent expansion

$$\phi(z) = z + \alpha_0 + \frac{\alpha_1}{z} + \cdots$$

about the point at infinity. The Faber polynomial of degree n is obtained by deleting all negative powers of z from the corresponding Laurent expansion of $[\phi(z)]^n$. For the unit disc the Faber polynomial of degree n is z^n and the corresponding Faber series for an analytic function is its Taylor series about the origin. Multiples of the

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Chebyshev polynomials are the Faber polynomials for an ellipse with foci at $(\pm 1, 0)$, and, in particular, for the real interval $[-1, 1]$.

Properties of the Faber polynomials and Faber series are described in the books of Markushevich [10, v. 3, pp. 104–112], Smirnov and Lebedev [12, Chapter 2] and Gaier [5, pp. 46–57], and in a survey article by Curtiss [2]. Markushevich [10] shows how Faber polynomials may be obtained for certain lemniscates, and Elliott [4] computed the coefficients of some Faber polynomials for the semidisc $|z| \leq 1$, $\operatorname{Re} z \geq 0$ and for the square $|\operatorname{Re} z| \leq 1$, $|\operatorname{Im} z| \leq 1$. Ellacott [3] pointed out that the trapezium rule could be used to compute the coefficients of Faber polynomials when the mapping function ϕ or its inverse is known. Thus the difficulty, for any particular region, lies in finding the appropriate conformal mapping.

The main theoretical results of this paper are summarized in the following three theorems.

THEOREM 1. *The complement of the unit disc $\{w: |w| \leq 1\}$ is mapped conformally onto the complement of the circular sector $\{z: |z| \leq 1, |\arg z| \leq \pi/\alpha\}$, with $\alpha > 1$, by*

$$\psi(w) = \frac{-\left[u + (u^2 - 1)^{1/2}\right]^2}{\left[v + (v^2 - 1)^{1/2}\right]^{p(a)}},$$

where

$$u(w) = \frac{i(w - 1)}{2aw^{1/2}}, \quad v(w) = \frac{(2 - a^2)(w - 1)^2 + 4wa^2}{a^2(w + 1)^2}$$

with $a = \alpha^{-1}(2\alpha - 1)^{1/2}$ and $p(a) = (1 - a^2)^{1/2}$.

THEOREM 2. *The transfinite diameter of the sector $\{z: |z| \leq 1, |\arg z| \leq \pi/\alpha\}$, with $\alpha \geq 1$, is*

$$\rho = \frac{\alpha^2}{(2\alpha - 1)^{2-1/\alpha}}.$$

THEOREM 3. *The coefficients of the Laurent expansion*

$$\psi(w) = \rho(w + \beta_0 + \beta_1 w^{-1} + \dots)$$

of the function defined in Theorem 1 may be generated recursively. Given α and p as in the statement of Theorem 1, let $x = 2p^2 - 1$, $a_0 = 1$ and, for $k \geq 1$,

$$a_k = P_k(x) + P_{k-1}(x),$$

where $P_n(x)$ is the Legendre polynomial of degree n . Then $\beta_0 = a_1$ and, for $k \geq 1$,

$$(k + 1)\beta_k = a_{k+1} - \sum_{\nu=0}^{k-1} \nu\beta_\nu a_{k-\nu}.$$

Theorems 1 and 2 are proved in Section 2, and Theorem 3 in Section 3. The numerical computation of coefficients of Faber polynomials for circular sectors is described in detail in Section 4, and in Section 5 the relationship of the norms of Faber and Chebyshev polynomials for circular sectors is discussed. Tables of coefficients of Faber polynomials, of degree up to 15, for selected sectors can be found in the Supplements section of this issue.

2. The Conformal Mapping. In this section we aim to calculate an analytic function $\psi(w)$ which maps the complement of the unit disc $\Delta = \{w: |w| \leq 1\}$ conformally onto the complement of the circular sector $S_h = \{z: |z| \leq 1, |\arg z| \leq 2h\}$, where $0 < h < \frac{1}{2}\pi$. Let J denote the interval $[-1, 1]$ of the real axis. Then the function $\frac{1}{2}(w^{-1} + w)$ maps $\mathbb{C} - \Delta$ conformally onto the slit plane $\mathbb{C} - J$ (see [8, p. 59]). If $\psi_0(z)$ is a function which maps $\mathbb{C} - J$ conformally onto $\mathbb{C} - S_h$, then $\psi(w) = \psi_0(\frac{1}{2}(w^{-1} + w))$ is the required function. It is therefore sufficient to calculate $\psi_0(z)$.

Let K denote the interval $(-\infty, 1]$ of the real axis. Then the cut plane $\mathbb{C} - K$ is mapped by the function $2^{-1/2}i(z-1)^{1/2}$ conformally onto the upper half-plane $\Pi = \{z: \operatorname{Im} z > 0\}$. A Schwarz-Christoffel transformation $\sigma(z)$ can be used to map Π conformally onto the shaded domain E shown in Figure 1. In [8, p. 160] this mapping is given by

$$(2) \quad \sigma(z) = \frac{i\pi}{2} - \cosh^{-1} \frac{z}{a} + \frac{(1-a^2)^{1/2}}{2} \cosh^{-1} \frac{(2-a^2)z^2 - a^2}{a^2(z^2 - 1)},$$

where $0 < a < 1$. The constant h in Figure 1 is given by

$$(3) \quad a = \pi^{-1}2(\pi h - h^2)^{1/2}, \quad h = \frac{1}{2}\pi[1 - (1-a^2)^{1/2}].$$

FIGURE 1

The Schwarz-Christoffel transformation $\sigma(z)$ given by Eq. (2) maps the upper half-plane conformally onto the shaded region E shown here.

Finally, the domain E is mapped by the function e^{-2z} conformally onto the domain obtained by cutting $\mathbb{C} - S_h$ along the negative real axis. The upper and lower boundary lines of E are both mapped by e^{-2z} onto the cut. The composition function $\psi_0(z) = \exp[-2\sigma(2^{-1/2}i(z-1)^{1/2})]$ therefore maps $\mathbb{C} - K$ conformally onto this cut version of $\mathbb{C} - S_h$.

Since $\cosh^{-1} \theta = \log[\theta + (\theta^2 - 1)^{1/2}]$, (2) can be written as

$$\sigma(z) = \frac{i\pi}{2} - \log \frac{z + (z^2 - a^2)^{1/2}}{a} + \frac{p(a)}{2} \log \frac{[(z^2 - a^2)^{1/2} + zp(a)]^2}{a^2(z^2 - 1)},$$

where $p(a) = (1 - a^2)^{1/2}$. This gives $\psi_0(z) = U(z)V(z)^{p(a)}$, where

$$(4) \quad U(z) = \frac{1}{2}a^{-2}[(z-1)^{1/2} + (z-1+2a^2)^{1/2}]^2,$$

$$(5) \quad V(z) = (z+1)a^2[(z-1+2a^2)^{1/2} + (z-1)^{1/2}p(a)]^{-2}.$$

It is easily seen that, in the slit plane $\mathbf{C} - J$, the functions $U(z)$, $V(z)$ are analytic and single-valued with $V(z) \neq 0$. Then $V(z)^{p(a)}$ is analytic in $\mathbf{C} - J$, though it might not be single-valued because $\mathbf{C} - J$ is not simply-connected. However, $V(z)^{p(a)}$ can only have branch points where $V(z) = 0$, and this does not happen at ∞ because (5) shows that $V(z) \rightarrow a^2[1 + p(a)]^{-2}$ as $z \rightarrow \infty$. Hence $V(z)^{p(a)}$ is single-valued in some neighborhood of ∞ and therefore single-valued in the whole of $\mathbf{C} - J$ by the monodromy theorem (see [10, v. 3, p. 269]). Thus $\psi_0(z)$ is analytic and single-valued in $\mathbf{C} - J$. It is easily seen that the part of K which lies in $\mathbf{C} - J$ is mapped by $\psi_0(z)$ onto the whole of the negative real axis. That is, $\psi_0(z)$ maps $\mathbf{C} - J$ conformally onto $\mathbf{C} - S_h$.

As shown above, $\mathbf{C} - \Delta$ is mapped conformally onto $\mathbf{C} - S_h$ by

$$\psi(w) = \psi_0\left(\frac{1}{2}(w^{-1} + w)\right) = U\left(\frac{1}{2}(w^{-1} + w)\right)V\left(\frac{1}{2}(w^{-1} + w)\right)^{p(a)}.$$

For computational convenience this can be written as

$$(6) \quad \psi(w) = \frac{-[u + (u^2 - 1)^{1/2}]^2}{[v + (v^2 - 1)^{1/2}]^{p(a)}},$$

where

$$(7) \quad u(w) = \frac{i(w-1)}{2aw^{1/2}}, \quad v(w) = \frac{(2-a^2)(w-1)^2 + 4wa^2}{a^2(w+1)^2}.$$

The appropriate branch for the square root $(u^2 - 1)^{1/2}$ is that for which

$$u^{-1}(u^2 - 1)^{1/2} \rightarrow 1 \quad \text{as } u \rightarrow +\infty.$$

Since (4) gives $z^{-1}U(z) \rightarrow 2a^{-2}$ as $z \rightarrow \infty$, it follows that

$$(8) \quad \lim_{w \rightarrow \infty} \frac{\psi(w)}{w} = \lim_{z \rightarrow \infty} \frac{\psi_0(z)}{2z} = a^{-2} \left[\frac{a}{1 + p(a)} \right]^{2p(a)} = \rho.$$

Now define $\phi(z) = \rho\psi^{-1}(z)$ where $w = \psi^{-1}(z)$ denotes the inverse mapping of $z = \psi(w)$. Then $\phi(z)$ maps $\mathbf{C} - S_h$ conformally onto the complement of the disc $\{w: |w| \leq \rho\}$. The number ρ is therefore the transfinite diameter of the sector S_h because (8) ensures that $\phi(z)$ satisfies (1). If the angle of the sector S_h is denoted by $2\pi/\alpha$, then $1 < \alpha = \pi/2h$ and (3) gives $a = \alpha^{-1}(2\alpha - 1)^{1/2}$. Then $p(a) = 1 - \alpha^{-1}$, and (8) gives

$$(9) \quad \rho = \frac{\alpha^2}{(2\alpha - 1)^{2-1/\alpha}}.$$

Some checks which confirm the accuracy of (6) and (9) will now be discussed. When $\alpha \rightarrow 1$, (6) gives $\psi(w) \rightarrow w$ and (9) gives $\rho \rightarrow 1$. These are the expected limits because $S_h \rightarrow \Delta$ as $\alpha \rightarrow 1$. When $\alpha \rightarrow +\infty$, (6) gives $\psi(w) \rightarrow (w+1)^2/4w$ and (9) gives $\rho \rightarrow 1/4$. These are the expected limits because S_h tends to the interval $[0, 1]$ of

the real axis when $\alpha \rightarrow +\infty$. When $\alpha = 2$, (9) gives $\rho = 4/3\sqrt{3}$ and (6) gives

$$\begin{aligned}
 \psi(w) &= -\left[u + (u^2 - 1)^{1/2}\right]^2 \left[v - (v^2 - 1)^{1/2}\right]^{1/2} \\
 &= \frac{\left[w - 1 + (w^2 + w + 1)^{1/2}\right]^2 \left[1 - w + 2(w^2 + w + 1)^{1/2}\right]}{w(w + 1)3\sqrt{3}} \\
 &= \frac{2(w^3 - 1) + 3(w^2 - w) + 2(w^2 + w + 1)^{3/2}}{w(w + 1)3\sqrt{3}}.
 \end{aligned}
 \tag{10}$$

In this case, S_h is the unit semidisc for which Elliott [4] obtained the transfinite diameter $\rho = 4/3\sqrt{3}$ by using a conformal mapping for which the appropriate inverse is

$$\psi_e(w) = i(b^{3/2} + c^{3/2})/(b^{3/2} - c^{3/2}),$$

where $b = w + e^{i\pi/3}$, $c = w + e^{-i\pi/3}$. This can be written as

$$\psi_e(w) = \frac{i(b^{3/2} + c^{3/2})^2}{b^3 - c^3} = \frac{i[b^3 + c^3 + 2(bc)^{3/2}]}{b^3 - c^3}.$$

Since $b^3 - c^3 = iw(w + 1)3\sqrt{3}$, $bc = 1 + w + w^2$ and $b^3 + c^3 = 2(w^3 - 1) + 3(w^2 - w)$, this and (10) give $\psi_e(w) = \psi(w)$. That is, Elliott [4] agrees with the above calculations.

3. The Laurent Expansion of $\psi(w)$ About the Point at Infinity. The function $\psi(w)$, given by Eq. (6), has the Laurent expansion

$$(11) \quad \psi(w) = \rho(w + \beta_0 + \beta_1 w^{-1} + \dots)$$

about the point at infinity. The presence of the coefficients of this expansion in a recurrence relation for the Faber polynomials (Eq. (17) below) provides the motivation for the derivation of a recurrence relation from which $\{\beta_k\}$ may be calculated.

Differentiation of (6) and (7) gives

$$\frac{d\psi}{dw} = \psi(w) \left[\frac{2u'}{\sqrt{u^2 - 1}} - \frac{pv'}{\sqrt{v^2 - 1}} \right]$$

with

$$u' = \frac{i(1 + w)}{4aw\sqrt{w}}, \quad v' = \frac{8p^2(w - 1)}{a^2(w + 1)^3},$$

and, since

$$\sqrt{v^2 - 1} = \frac{2pu\sqrt{u^2 - 1}}{a^2u^2 - 1},$$

this finally reduces to

$$(12) \quad \frac{d\psi}{dw} = \frac{\psi(w)}{w} \left[1 - \frac{4p^2w}{(w + 1)^2} \right]^{1/2}.$$

It is now convenient to let $\zeta = w^{-1}$ and $\Psi(\zeta) = \psi(w)$, so that (12) becomes

$$(13) \quad \Psi(\zeta) = -(1 - 2x\zeta + \zeta^2)^{-1/2}(1 + \zeta)\zeta \frac{d\Psi}{d\zeta},$$

where $x = 2p^2 - 1$. Then $-1 < x < 1$ because $p = 1 - \alpha^{-1}$ and $\alpha > 1$. For $|\zeta| < 1$,

$$(1 - 2x\zeta + \zeta^2)^{-1/2} = \sum_{n=0}^{\infty} P_n(x)\zeta^n,$$

where $P_n(x)$ is the Legendre polynomial of degree n , and (13) gives

$$(14) \quad \Psi(\zeta) = \left[\sum_{k=0}^{\infty} a_k \zeta^k \right] \left[-\zeta \frac{d\Psi}{d\zeta} \right],$$

where $a_0 = 1$ and, for $k \geq 1$,

$$(15) \quad a_k = P_k(x) + P_{k-1}(x).$$

From (11),

$$\Psi(\zeta) = \rho \left[\zeta^{-1} + \sum_{\nu=0}^{\infty} \beta_{\nu} \zeta^{\nu} \right]$$

for $|\zeta| < 1$. By substituting this in (14) and equating the coefficients of ζ^k on both sides, we find that $\beta_0 = a_1$ and, for $k \geq 1$,

$$(16) \quad (k+1)\beta_k = a_{k+1} - \sum_{\nu=0}^{k-1} \nu \beta_{\nu} a_{k-\nu}.$$

The Legendre polynomials, and hence the coefficients a_k , may be generated by using the recurrence relation

$$(n+1)P_{n+1}(x) - (2n+1)xP_n(x) + nP_{n-1}(x) = 0.$$

4. Computational Details. The Faber polynomials ϕ_n satisfy the recurrence relation

$$(17) \quad \phi_{n+1}(z) = z\phi_n(z) - \sum_{k=0}^{n-1} b_k \phi_{n-k}(z) - (1+n)b_n, \quad n > 0$$

(see, e.g., Ellacott [3]), with $b_k = \beta_k \rho^{k+1}$, where ρ is the transfinite diameter of the region of interest and β_k is a coefficient of the Laurent expansion (11). In particular, for a sector of half-angle π/α , Eq. (15) and the recurrence relation (16) give

$$(18) \quad \begin{aligned} a_1 &= 1 + x, \quad a_2 = \tfrac{1}{2}(1+x)(3x-1), \quad a_3 = \tfrac{1}{2}(1+x)(5x^2-2x-1), \\ b_0 &= \rho(1+x), \quad b_1 = \rho^2(1+x)(3x-1)/4, \\ b_2 &= -\rho^3(1-x^2)(7x+1)/12 \end{aligned}$$

with $x = 1 - 2a^2$ and $a = \alpha^{-1}(2\alpha - 1)^{1/2}$. It follows that the Faber polynomials of degree ≤ 3 are

$$(19a) \quad \phi_0(z) = 1,$$

$$(19b) \quad \phi_1(z) = z - 2\rho(1 - a^2),$$

$$(19c) \quad \phi_2(z) = z^2 - 4\rho(1 - a^2)z + 2\rho^2(1 - a^4),$$

and

$$(19d) \quad \begin{aligned} \phi_3(z) &= z^3 - 6\rho(1 - a^2)z^2 + 3\rho^2(1 - a^2)(3 - a^2)z \\ &\quad - 2\rho^3(1 - a^2)(2a^4 + 1). \end{aligned}$$

Faber polynomials of higher degree could also be generated in this way but we chose to base our computations on an alternative numerical method which is more versatile and permits independent checks on its accuracy.

The coefficients of a Faber polynomial of degree n ,

$$\phi_n(z) = \sum_{k=0}^n C_k^{(n)} z^k,$$

may be expressed in a number of ways in terms of the relevant mapping (see, e.g., Ellacott [3]). In particular,

$$(20) \quad C_k^{(n)} = \frac{\rho^n}{2\pi i} \oint_{|w|=R} \frac{w^n (d\psi/dw)}{[\psi(w)]^{k+1}} dw$$

for any $R > 1$. This differs by a factor of ρ^n from the expression quoted by Ellacott [3] because in his notation ψ maps the complement of the disc $\{w: |w| \leq \rho\}$, rather than that of the unit disc, onto the region of interest in the z -plane.

Equation (12) gives the derivative of ψ in a convenient form and, when this is used, Eq. (20) becomes

$$(21) \quad C_k^{(n)} = \frac{(R\rho)^n}{2\pi} \int_0^{2\pi} F_k(R e^{i\theta}) \exp(in\theta) d\theta,$$

where

$$(22) \quad F_k(w) = \left[1 - \frac{4p^2 w}{(w+1)^2} \right]^{1/2} / [\psi(w)]^k.$$

Since the integrand in (21) is a periodic function which is integrated over a period, $C_k^{(n)}$ may be computed efficiently by the trapezium rule, which gives

$$(23) \quad C_k^{(n)} \simeq \frac{(R\rho)^n}{N} \sum_{m=0}^{N-1} F_k(R \exp(i\theta_m)) \exp(in\theta_m)$$

with $\theta_m = 2\pi m/N$, when N is the number of equal subintervals used.

For a given value of n the coefficients $C_k^{(n)}$, for $k = 0, 1, \dots, n$, may be calculated from (23) using a suitable value of N , but this is inefficient if more than one Faber polynomial is to be found. The values of w used in (22) depend on the choice of R and N but not on n . When R and N are chosen, the calculation of the coefficients $C_k^{(n)}$, for Faber polynomials of degree $n_{\min}$ to $n_{\max}$, may be arranged as follows.

1. *Preliminary calculation.*

For $m = 0, 1, \dots, N-1$:

Calculate $w_m = R \exp(i\theta_m)$.

Calculate and store $\psi(w_m)$ and the numerator of the expression in (22), with $w = w_m$.

2. *Computation of coefficients.*

For $k = 0, 1, \dots, n$:

2.1. For $m = 0, 1, \dots, N-1$:

Calculate $F_k(w_m)$ from stored data.

2.2. For $n = n_{\min}, \dots, n_{\max}$:

Calculate $C_k^{(n)}$ from (23).

This arrangement, in which $C_k^{(n)}$ is calculated for a given k and all relevant n , would allow the use of a Fast Fourier Transform algorithm for the step 2.2, as suggested by Lyness and Sande [9] for the evaluation of Taylor coefficients, and by Ellacott [3] in connection with another formula for the coefficients of Faber polynomials.

Properties of the Faber polynomials provide a number of ways of assessing the accuracy of computed coefficients.

(i) By definition, the Faber polynomials are monic, so $C_n^{(n)} = 1$ for each n . Computation of these coefficients provides a particularly valuable check, as it turns out that for any n the coefficient most sensitive to discretization error is $C_n^{(n)}$; Eq. (22) shows that this is to be expected since a higher power of $z = \psi(w)$ occurs in $F_n(w)$ than in $F_k(w)$ for $k < n$.

(ii) It is readily seen that $C_{n-1}^{(n)} = -nb_0$, and the recurrence relation (17) gives

$$C_{n-2}^{(n)} = C_{n-3}^{(n-1)} - b_0 C_{n-2}^{(n-1)} - b_1$$

and

$$C_{n-3}^{(n)} = C_{n-4}^{(n-1)} - b_0 C_{n-3}^{(n-1)} - b_1 C_{n-3}^{(n-2)} - b_2.$$

Thus, knowing b_0 , b_1 and b_2 from (18) we have an alternative method of evaluating the coefficients of z^{n-1} , z^{n-2} and z^{n-3} in $\phi_n(z)$. In particular, from the equations (19), the polynomials $\phi_1(z)$, $\phi_2(z)$ and $\phi_3(z)$ are known for any sector.

(iii) For a sector of half-angle π/α , with α rational, a^2 is a rational number and, therefore, so also are the coefficients $\beta_0, \beta_1, \dots$ of the Laurent expansion (11). It follows from the recurrence relation (17) that $C_k^{(n)} \rho^{k-n}$ is a rational number. Tabulation of this quantity provides a valuable visual check, particularly for $\alpha = 2$ or 4.

(iv) The coefficients $C_k^{(n)}$ are real but, since the sum in (23) involves complex quantities, the imaginary part of the computed result will not be exactly zero. However, this does not provide a useful check as the size of the imaginary part obtained gives no indication of the magnitude of the discretization error in the real part.

Although in principle any $R > 1$ may be used in (23), the choice of R was found to have a very significant effect on the accuracy of the results obtained for a given N , the number of terms in the sum. A study of the results of our computations in double- and quadruple-precision leads to the following conclusions.

(a) The discretization error is dramatically decreased by increasing N or R . With $R = 3$ and $N = 128$, the coefficients of the Faber polynomials of degree ≤ 15 , for the sectors investigated, were correct to all 25 digits printed by the quadruple-precision program. However, for a sector of half-angle 5° , with $N = 128$, the calculated value of the unit coefficient $C_{15}^{(15)}$ is in error by 1.4×10^{-7} when $R = 2$, and calculations with $R = 1.5$ return the ridiculous value 1.4×10^9 instead of 1. For the same sector, with $R = 3$, the computed value of $C_{15}^{(15)}$ is in error by 3.9×10^{-7} when $N = 64$, and is correct to more than 25 digits when $N = 128$, as already mentioned, but becomes 1.4×10^3 when $N = 32$; thus a four-fold increase in N reduces the error in this case by more than 28 orders of magnitude.

(b) For any given sector, and given values of N and R , the discretization error increases with the degree of the polynomial, and for a polynomial of degree n it is greatest for the unit coefficient $C_n^{(n)}$. For example, when $R = 3$ and $N = 32$, although $C_{15}^{(15)}$ for the sector of half-angle 5° is returned as 1.4×10^3 , the error in the calculated value of $C_0^{(15)}$ is merely 9×10^{-24} , making that coefficient correct to 15 significant digits; the corresponding errors in the unit coefficients $C_{10}^{(10)}$, $C_5^{(5)}$ and $C_1^{(1)}$ are 4.9×10^{-2} , 7.9×10^{-7} , and 4.8×10^{-13} , respectively.

(c) The discretization error increases, for given values of N and R , as the angle of the sector is decreased. When $N = 64$ and $R = 3$, for example, the discretization errors in the computed values of $C_{15}^{(15)}$ for sectors of half-angle 5° , 10° , 30° and 90° are, respectively, 3.9×10^{-7} , 9.4×10^{-8} , 2.9×10^{-10} , and 2.3×10^{-18} .

(d) As R is increased, the image, under the mapping ψ , of the circle $|w| = R$ becomes more nearly circular. As this happens, rounding error becomes increasingly apparent in double-precision calculations, and it was evidence of this rounding error which prompted the quadruple-precision calculations. For any given sector the rounding error increases with increasing R , and for any given R it is greater for the unit semidisc than for any smaller sector, which is consistent with the fact that the images of $|w| = R$ become nearly circular more rapidly for the unit semidisc than for smaller sectors. For example, for the unit semidisc, the rounding error in the value of $C_0^{(15)}$, calculated in double-precision with $N = 128$, is 2.5×10^{-10} when $R = 4$ and 1.0×10^{-14} when $R = 2$; the corresponding errors in $C_0^{(15)}$ for a sector of half-angle 30° are 2.2×10^{-14} and 1.0×10^{-17} , respectively.

5. The Faber Polynomials for Circular Sectors. A supplement to this paper contains the coefficients of the Faber polynomials, of degree 1 to 15, for symmetric sectors of the unit disc of half-angle 5° , 10° , 15° , 30° , 45° and 90° . The polynomials for sectors of radius other than 1, and for angular ranges of the form $\theta \leq \arg z \leq \phi$, may be obtained, if required, by simple changes of variable. The tabulated coefficients are believed to be correct to the number of figures quoted, having been obtained by rounding to 14 decimal places results which all our tests show to be accurate to 25 decimal digits. Comparison with previous work is possible only in the case of the semidisc for which Elliott [4] computed the coefficients of the Faber polynomials of degree ≤ 9 . The numbers in Table 6 of the supplement agree with Elliott's except that there is a misprint in his $C_0^{(9)}$ and there is an occasional discrepancy of one unit in the last decimal place which he quotes.

Coleman [1] used the Faber polynomials tabulated here, in conjunction with the Lanczos τ -method, to obtain near-minimax polynomial approximations for analytic functions on circular sectors. In that work a Faber polynomial appears as a perturbation term in a differential equation, and consequently the maximum value of the modulus of the polynomial is of interest. In particular, it is useful to have a comparison with the Chebyshev polynomial (T -polynomial) of degree n , which is the monic polynomial

$$T_n(z) = z^n + a_{n-1}z^{n-1} + a_{n-2}z^{n-2} + \cdots + a_0$$

of smallest maximum modulus on the sector of interest.

An upper bound on the norm of a Faber polynomial,

$$\|\phi_n\|_\infty = \max_{z \in D} |\phi_n(z)|,$$

where $D = \{z: |z| \leq 1, |\arg z| \leq \pi/\alpha\}$, with $\alpha \geq 2$, may be obtained from the work of Pommerenke [11]. His Satz 3, expressed in our notation, shows that for a convex region of transfinite diameter ρ ,

$$(24) \quad \rho^n \leq \|\phi_n\| \leq 2\rho^n.$$

Furthermore, if $\pi\beta$ is the largest exterior angle of the region, then as $n \rightarrow \infty$

$$(25) \quad \rho^{-n} \|\phi_n\| \rightarrow \beta;$$

for our sector D , $\beta = \max\{2(1 - \alpha^{-1}), 3/2\}$. As $\alpha \rightarrow \infty$, so that the sector becomes the interval $[0, 1]$, the upper bound in (24) is attained, as then $\rho = 1/4$, the Faber polynomial of degree n is a multiple of a shifted Chebyshev polynomial

$$\phi_n(x) = 2^{1-2n} T_n^*(x),$$

and $\max_{x \in [0,1]} |T_n^*(x)| = 1$. The values of $\rho^{-n} \|\phi_n\|$ given in Table 1 show that for each of the sectors considered, this quantity is nearly constant but no obvious pattern is evident in its approach to the limit given by (25).

Table 2, which is based on the work of Grothkopf and Opfer [7], shows $\rho^{-n} \|T_n\|$ for the same sectors, with $n \leq 6$; results for T -polynomials of higher degree are not available. In the range of this table, $\|\phi_n\| \leq 1.5 \|T_n\|$. Furthermore, since it is known (Walsh [13, p. 320]) that $\|T_n\| \geq \rho^{-n}$, we can conclude from (24) that for all n ,

$$\|\phi_n\| \leq 2 \|T_n\|.$$

To use the Faber polynomials in the Lanczos τ -method, it is necessary to have explicit expressions in powers of z , as provided by the tables in the supplement.

TABLE 1

Values of $\|\phi_n\| \rho^{-n}$, the scaled norms of Faber polynomials of degree 1 to 15, and the limit as $n \rightarrow \infty$. The column headings show the half-angles of the sectors to which they refer.

n	5°	10°	15°	30°	45°	90°
1	1.890	1.784	1.681	1.389	1.347	1.392
2	1.994	1.977	1.949	1.813	1.617	1.532
3	1.902	1.826	1.766	1.648	1.575	1.469
4	1.979	1.925	1.855	1.622	1.442	1.479
5	1.920	1.876	1.844	1.702	1.497	1.507
6	1.960	1.884	1.811	1.669	1.535	1.486
7	1.937	1.903	1.852	1.644	1.500	1.490
8	1.945	1.874	1.827	1.681	1.486	1.503
9	1.949	1.899	1.828	1.673	1.505	1.492
10	1.938	1.886	1.844	1.652	1.515	1.494
11	1.952	1.886	1.824	1.672	1.493	1.502
12	1.938	1.896	1.836	1.674	1.497	1.494
13	1.949	1.882	1.837	1.658	1.508	1.496
14	1.942	1.893	1.826	1.667	1.506	1.501
15	1.944	1.888	1.839	1.674	1.492	1.496
∞	1.944	1.889	1.833	1.667	1.500	1.500

TABLE 2

Values of $\|T_n\| \rho^{-n}$, the scaled norms of T -polynomials of degree 1 to 6. The column headings show the half-angles of the sectors to which they refer.

n	5°	10°	15°	30°	45°	90°
1	1.734	1.576	1.464	1.301	1.331	1.299
2	1.564	1.480	1.645	1.693	1.468	1.398
3	1.578	1.675	1.566	1.359	1.465	1.317
4	1.677	1.486	1.357	1.322	1.268	1.220
5	1.583	1.366	1.354	1.239	1.208	1.164
6	1.469	1.356	1.269	1.195	1.177	1.128

However, if numerical values of the Faber polynomials are required, as for example in summing Faber series, that form is not ideal. The tabulated coefficients and the upper bound in (24) show that the norm of a Faber polynomial may be much smaller than the magnitudes of some of its coefficients; significant cancellation would then occur if those coefficients were used to evaluate the polynomial. The alternative is to use the recurrence relation (17), with coefficients β_k computed as described in Section 3, to generate $\{\phi_n(z)\}$ numerically for each required value of z .

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Supplement to The Faber Polynomials for Circular Sectors

By John P. Coleman and Russel A. Smith

Tables of coefficients of Faber polynomials

$$\Phi_n(z) = \sum_{k=0}^n c_k^{(n)} z^k,$$

for circular sectors.

TABLE 1

COEFFICIENTS OF FABER POLYNOMIALS FOR A SECTOR OF HALF ANGLE 5 DEGREES

	n=1	n=2	n=3	n=4	n=5
C (0)	-0.54710820750846	0.16701246657898	-0.04680954204779	0.01388005930428	-0.00389765187932
C (1)	1.00000000000000	-1.09421641501692	0.69950978595315	-0.35339015330471	0.15797430671061
C (2)		1.00000000000000	-1.64132462252538	1.53133449605045	-1.07958360017665
C (3)			1.00000000000000	-2.18843283003384	2.66248659687086
C (4)				1.00000000000000	-2.73554103754230
C (5)					1.00000000000000
	n=6	n=7	n=8	n=9	n=10
C (0)	0.00115160659462	-0.00032944500845	0.00009571763079	-0.00002775568542	0.00000798714894
C (1)	-0.06513782570752	0.02544447071205	-0.00954620177328	0.00347373593915	-0.00123393522660
C (2)	0.64268779492266	-0.34119471013575	0.16675290315018	-0.07654197695835	0.03344621778040
C (3)	-2.38644435486032	1.7669984979219	-1.14254426986018	0.66849329519433	-0.36200338323504
C (4)	4.09296608841440	-4.44373688955242	3.91948668400808	-2.98142146292353	2.02812716271008
C (5)	-3.28264924505076	5.82277279068105	-7.40922567644968	7.57832139709631	-6.62083943287081
C (6)	1.00000000000000	-3.82975745255922	7.85190724367083	-11.44867518774879	13.31127397541997
C (7)		1.00000000000000	-4.37686566006769	10.18036890738373	-16.72584989564648
C (8)			1.00000000000000	4.92397386757615	-12.80815796181974
C (9)				1.00000000000000	-5.47108207508461
C (10)					1.00000000000000
	n=11	n=12	n=13	n=14	n=15
C (0)	-0.00000232855241	0.00000066910250	-0.0000019473834	0.0000005617161	-0.0000001627021
C (1)	0.00042980247386	-0.00014732336691	0.00004981542261	-0.00001665181861	0.00000551102608
C (2)	-0.01404639095742	0.00570932212981	-0.00225795059077	0.00087243116326	-0.00033040208086
C (3)	0.18428516445223	-0.08919012387962	0.04138478286789	-0.01852946197285	0.00804602694502
C (4)	-1.26377400048633	0.73358679890229	-0.40159066405923	0.20926779472501	-0.10455359281036
C (5)	5.12843644705294	-3.61080434309925	2.35191348418737	-1.43576081093505	0.82963468636079
C (6)	-13.12360870090515	11.39561761833194	-8.94035342328565	6.45348743834503	-4.34425532062840
C (7)	21.775711129217926	-23.90135635804360	22.98419458102702	-19.87311469739459	15.73973721542796
C (8)	-23.40451427233946	33.71859710741151	-40.76354525727285	42.96875038196038	-40.60093918209988
C (9)	15.73527440697888	-31.64843279002442	49.97649206799115	-65.96649320570513	75.682477720662159
C (10)	-6.01819028259367	18.96171824286114	-41.62136992089810	71.47555370762930	-102.26239215673389
C (11)	1.00000000000000	-6.56529849010153	22.48748946946652	-53.48709013715719	99.23153644687584
C (12)		1.00000000000000	-7.11240669760999	26.31258808679502	-67.40935791099841
C (13)			1.00000000000000	-7.65951490511845	30.43701409484665
C (14)				1.00000000000000	-8.20662311262691
C (15)					1.00000000000000

TABLE 2

COEFFICIENTS OF FABER POLYNOMIALS FOR A SECTOR OF HALF ANGLE 10 DEGREES

	n=1	n=2	n=3	n=4	n=5
C (0)	-0.57487484798296	0.20526420694254	-0.06109049603599	0.02076322442583	-0.00652002217240
C (1)	1.00000000000000	-1.14974965956591	0.803617946667896	-0.44411329881276	0.21836834021236
C (2)		1.00000000000000	-1.72462454394887	1.73245277725879	-1.32510786507168
C (3)			1.00000000000000	-2.29949939193182	2.99176869868206
C (4)				1.00000000000000	-2.87437423991478
C (5)					1.00000000000000
	n=6	n=7	n=8	n=9	n=10
C (0)	0.00210990612744	-0.00068654420672	0.00021794177399	-0.00007115999598	0.00002277193218
C (1)	-0.09926134193797	0.04279087619782	-0.01774784426625	0.00714295963392	-0.00280882451516
C (2)	0.86027362404295	-0.49974331194781	0.26788866169690	-0.13511934846973	0.06497009663287
C (3)	-2.89408946167261	2.32127736296250	-1.63346870098535	1.04305377717430	-0.61739243828172
C (4)	4.58156571094875	-5.34095335547540	5.08539559542092	-4.19229424280761	3.10003953254937
C (5)	-3.44924908789774	6.50184381405887	-8.85577481333991	9.74586211127323	-9.19721717438123
C (6)	1.00000000000000	-4.02412393588069	8.75260300801241	-13.62850910212600	17.00512845177949
C (7)		1.00000000000000	-4.59899878386365	11.33384329280938	-19.849.4148869351
C (8)			1.00000000000000	-5.17387363184660	14.24556466844978
C (9)				1.00000000000000	-5.74874847982956
C (10)					1.00000000000000
	n=11	n=12	n=13	n=14	n=15
C (0)	-0.0000033756756	0.00000237720618	-0.0000076043088	0.0000024654727	-0.0000007923425
C (1)	0.0010836763151	-0.00041156745676	0.00015427843702	-0.0000518373985	0.00002099250023
C (2)	-0.03005905249512	0.01347265493786	-0.00588002399896	0.0025890015027	-0.00104986012680
C (3)	0.3445958318040	-0.18299776869924	0.0932823238930	-0.04592954422096	0.02195130014804
C (4)	-2.10487691230869	1.33396005860829	-0.79857332697095	0.45560966729401	-0.249608570454680
C (5)	7.71907867661002	-5.90347948124036	4.18551374224731	-2.78606339405455	1.75802613964680
C (6)	-18.06116717411848	16.94735444213540	-14.40436480431009	11.28849225084430	-8.26511229519032
C (7)	27.67486390960481	-32.65176590011330	33.8535659264235	-31.63993883092097	27.14559850035367
C (8)	-27.70765723399231	42.67595552881937	-55.35416752837731	62.8185882705575	-64.09543021108418
C (9)	17.48776713493033	-37.39404162261226	63.03850810489844	-89.861379129107582	109.86222624820260
C (10)	-6.32362332781251	21.06045069226086	-49.09827990368320	89.90184418472229	-137.59913501476391
C (11)	1.00000000000000	-6.8949817579547	24.96361534043154	-63.01935734997500	124.51450406657632
C (12)		1.00000000000000	-7.47337302377843	29.19726107944564	-79.32025922834752
C (13)			1.00000000000000	-8.04824787176138	33.76138790930317
C (14)				1.00000000000000	-8.62312271974434
C (15)					1.00000000000000

TABLE 3

COEFFICIENTS OF FABER POLYNOMIALS FOR A SECTOR OF HALF ANGLE 15 DEGREES.

	n= 1	n= 2	n= 3	n= 4	n= 5
C (0)	-0.59406916854258	0.24354270893037	-0.07802203174563	0.02895917861573	-0.01017591832985
C (1)	1.00000000000000	-1.18813833708516	0.89469132891486	-0.53316367684631	0.28390692207496
C (2)		1.00000000000000	-1.78220750562774	1.89875812591220	-1.55230215250907
C (3)			1.00000000000000	-2.37627667417031	3.25574309992245
C (4)				1.00000000000000	-2.97034584271289
C (5)					1.00000000000000
	n= 6	n= 7	n= 8	n= 9	n=10
C (0)	0.00353302335241	-0.00127750642102	0.00044542096664	-0.00015754674676	0.00005619420919
C (1)	-0.14021078393944	0.06571312514715	-0.02967934423999	0.01301870802773	-0.00558211128981
C (2)	1.08261665113688	-0.67796360589007	0.39269796222477	-0.21441983124714	0.11177002804837
C (3)	-3.34509526671549	2.86539243825745	-2.16170842768742	1.48408141840011	-0.94715541453437
C (4)	4.96564625094555	-6.12120082744717	6.19708959555868	-5.45381670801380	4.31848695147800
C (5)	-3.56441501125547	7.02846757898152	-10.09027664268572	11.76711467482870	-11.81474937211755
C (6)	1.00000000000000	-4.15848417979805	9.44420708403037	-15.46198052041273	20.38942546752172
C (7)		1.00000000000000	-4.75255334834063	12.21286476609208	-22.44597026860980
C (8)			1.00000000000000	-5.34662251688321	15.33444062516666
C (9)				1.00000000000000	-5.94069168542578
C (10)					1.00000000000000
	n=11	n=12	n=13	n=14	n=15
C (0)	-0.00001964737368	0.00000698957833	-0.00000247278584	0.00000086890895	-0.00000030921185
C (1)	0.00235018289705	-0.00097438193179	0.00039888037227	-0.00016152448954	0.00006479423083
C (2)	-0.05612343610562	0.02732696996662	-0.01296665397453	0.00601911821699	-0.00274178141732
C (3)	0.57026163591187	-0.32735978527466	0.18059968924528	-0.09633639859394	0.04992509530893
C (4)	-3.14745876593611	2.14536840943601	-1.38360088453866	0.85173342527396	-0.50389460487173
C (5)	10.58324884659231	-8.66065274767496	6.58402923831536	-4.70761330223495	3.19562642306497
C (6)	-22.97704886320235	22.94804986599264	-20.81415761147054	17.44469971672226	-13.68485320281819
C (7)	33.00253100475802	-41.21933119381668	45.38251529527867	-45.15846457100129	41.34078309995714
C (8)	-31.25190369525853	50.66949155732398	-69.44027799724315	83.51776338608219	-90.41884888760900
C (9)	18.0893466125411	-42.08943860834052	74.57791863567208	-111.23262857888789	145.05191219519673
C (10)	-6.53476085396836	22.63634687435444	-55.16823281583736	106.03997498992087	-170.95717196766994
C (11)	1.00000000000000	-7.12883002251094	26.81667276446763	-70.69794412573066	146.49237460985500
C (12)		1.00000000000000	-7.72289919105352	31.34992583159370	-88.88823034600201
C (13)			1.00000000000000	-8.31696835959610	36.23609257573263
C (14)				1.00000000000000	-8.91103752813868
C (15)					1.00000000000000

TABLE 4

COEFFICIENTS OF FABER POLYNOMIALS FOR A SECTOR OF HALF ANGLE 30 DEGREES.

	n= 1	n= 2	n= 3	n= 4	n= 5
C (0)	-0.61624027909633	0.35696695668587	-0.14396819888129	0.06287512285754	-0.02927459383730
C (1)	1.00000000000000	-1.23248055819265	1.10507855739989	-0.78792478503473	0.50559256223451
C (2)		1.00000000000000	-1.84872083728898	2.23294223969462	-2.11989584568587
C (3)			1.00000000000000	-2.46496111638530	3.74055800357007
C (4)				1.00000000000000	-3.08120139548163
C (5)					1.00000000000000
	n= 6	n= 7	n= 8	n= 9	n=10
C (0)	0.01273113115990	-0.00556367359579	0.00252412717636	-0.0011511936476	0.00048852699560
C (1)	-0.30441829450865	0.17459489041304	-0.09670549394607	0.05222685612677	-0.02762229143011
C (2)	1.74210376484482	-1.29926707037639	0.90285353698961	-0.59459584632459	0.37546471651054
C (3)	-4.373899090957541	4.33627625663619	-3.83122931193459	3.10734569602923	-2.35858098169410
C (4)	5.62792584902624	-7.78395550544407	8.99618920702123	-9.15139424395587	8.45543318781628
C (5)	-3.69744167457796	7.89504577606312	-12.58408116203256	16.57413342887741	-19.03340094890922
C (6)	1.00000000000000	-4.31368195367428	10.54191778468073	-19.0045940808160	28.06661137854712
C (7)		1.00000000000000	-4.92992223277061	13.56854187487905	-27.29061677233189
C (8)			1.00000000000000	-5.4616251186693	16.97491804665808
C (9)				1.00000000000000	-6.16240279096326
C (10)					1.00000000000000
	n=11	n=12	n=13	n=14	n=15
C (0)	-0.00021930668382	0.00009745650633	-0.00004280821236	0.00001910352444	-0.00000851011536
C (1)	0.01436192784051	-0.0073670704200	0.00373541285619	-0.00187504529623	0.00093331411241
C (2)	-0.22918035643688	0.13602909117965	-0.07886952223321	0.04482610621411	-0.02504354497935
C (3)	1.69794428696546	-1.17055230540288	0.77835219814176	-0.50197119684237	0.31534220059842
C (4)	-7.24452142626779	5.83998841970779	-4.47658006531314	3.28918590018436	-2.33094495575296
C (5)	19.69237435777460	-18.75976573232356	16.70967879192726	-14.07419841939834	11.30634801009672
C (6)	-35.86230739037765	41.01646207825618	-42.94828693004128	41.83513775500772	-38.35981101160440
C (7)	44.61433715583762	-67.52345943647601	78.50892642212381	-89.53972987699394	94.59795810735711
C (8)	-37.66506378352415	62.50223650402107	-103.49135988326869	140.61860200812766	-173.39611770192357
C (9)	20.761043630001784	-50.36565497039909	98.15944680983451	-162.9185377818740	238.70136001807591
C (10)	-6.77864307005959	24.92692663495831	-65.62640886169742	138.15931710347986	-246.72441594344885
C (11)	1.00000000000000	-7.39488334915591	29.47255905147951	-83.68134398615986	189.21940805862394
C (12)		1.00000000000000	-8.01112362825224	34.39794354958142	-104.76447887252711
C (13)			1.00000000000000	-8.62736390734856	39.70308012926404
C (14)				1.00000000000000	-24.360418644489
C (15)					1.00000000000000

TABLE 5

COEFFICIENTS OF FABER POLYNOMIALS FOR A SECTOR OF HALF ANGLE 45 DEGREES.

	n= 1	n= 2	n= 3	n= 4	n= 5
C (0)	-0.59751792062368	0.45620201698490	-0.23308324570747	0.11476996343846	-0.06283659387978
C (1)	1.00000000000000	-1.19503584124735	1.21984452367701	-0.99817507606000	0.73580857344425
C (2)		1.00000000000000	-1.79255376187103	2.34051469583556	-2.46251790662695
C (3)			1.00000000000000	-3.9007168249471	3.18121253346056
C (4)				1.00000000000000	-2.98758960311838
C (5)					1.00000000000000
	n= 6	n= 7	n= 8	n= 9	n=10
C (0)	0.03446029421878	-0.01788656826698	0.00935345793435	-0.00506237103358	0.00270704199080
C (1)	-0.51355561831726	0.34430264083090	-0.2232076574083	0.14140357979144	-0.08797935198853
C (2)	2.27361898528674	-1.92494840317540	1.53042742978887	-1.15948081562388	0.84578473032532
C (3)	-4.83944027104494	5.29118819539478	-5.21822193566418	4.76666179818875	-4.10282194237149
C (4)	5.65293803655200	-8.34227322913461	10.47897195410561	-11.73772134065940	12.05942474755255
C (5)	-3.58510752374206	7.84469120510988	-13.18434720917059	18.65489476566494	-23.32709474548254
C (6)	1.00000000000000	-4.18262544436573	10.39347203913420	-19.57899263942752	30.7643988822684
C (7)		1.00000000000000	-4.78014336498941	13.29928053862497	-27.73953994818003
C (8)			1.00000000000000	-5.37766128561309	16.56211670358217
C (9)				1.00000000000000	-5.97517920623676
C (10)					1.00000000000000
	n=11	n=12	n=13	n=14	n=15
C (0)	-0.00141629997009	0.00075086371767	-0.00040362691494	0.00021410937758	-0.00011266286780
C (1)	0.05392683488188	-0.03262650102974	0.01953527471243	-0.01159730940013	0.00683165327009
C (2)	-0.59847238201031	0.41298354225828	-0.27903527817758	0.18518164127564	-0.12101593577260
C (3)	3.36748356118296	-2.65851755126155	2.03183128797249	-1.51077030362851	1.09713931404376
C (4)	-11.57764261091221	10.52247837795972	-9.14018666922472	7.64823902673099	-6.18635429573099
C (5)	26.55239045111462	-28.05743638627881	27.90624212015984	-26.39268287188514	23.91962153408321
C (6)	-42.40545814468061	52.87666143273587	-60.87925534349887	65.66420274771792	-67.06389392179792
C (7)	47.88019933385385	-72.04356026480598	97.54645161744575	-121.39827799160778	140.96994424188730
C (8)	-37.87931956630276	71.20277386851688	-116.03994742919626	169.40027925361222	-226.40977467564709
C (9)	20.18198053400582	-50.21166191427034	102.05987301209530	-178.99712842275411	280.08766970673940
C (10)	-6.57269712686044	24.1588720289591	-64.94989742815740	141.90676503837687	-266.39773935672713
C (11)	1.00000000000000	-7.17021504748412	28.49279119125244	-82.30735653363858	192.32618697505777
C (12)		1.00000000000000	-7.76773296810779	33.18373801807542	-102.49736965898851
C (13)			1.00000000000000	-8.36525088873147	38.23171251036484
C (14)				1.00000000000000	-8.96276880935515
C (15)					1.00000000000000

TABLE 6

COEFFICIENTS OF FABER POLYNOMIALS FOR A SECTOR OF HALF ANGLE 90 DEGREES.

	n= 1	n= 2	n= 3	n= 4	n= 5
C (0)	-0.38490017945975	0.51851851851852	-0.48468911487524	0.38134430727023	-0.27771947105052
C (1)	1.00000000000000	-0.76980035891950	1.00000000000000	-1.08342272736819	1.05624142661180
C (2)		1.00000000000000	-1.1547005387925	1.62962962962963	-1.99577870830982
C (3)			1.00000000000000	-1.53960071783900	2.40740740740741
C (4)				1.00000000000000	-1.92450089729875
C (5)					1.00000000000000
	n= 6	n= 7	n= 8	n= 9	n=10
C (0)	0.20220494843266	-0.15401482565793	0.12182349498815	-0.09652180941365	0.07474325396352
C (1)	-0.96937822975048	0.86241934664431	-0.75575990122240	0.65569272976680	-0.56282057548848
C (2)	2.22633744855967	-2.33210437952499	2.33988721231520	-2.2766608207194	2.16357036811236
C (3)	-3.72877930650899	4.06172839506173	-4.70116762401868	5.17421124828532	-5.47929383977240
C (4)	3.33333333333333	-4.98944677077454	6.75445816186557	-8.49631507251894	10.10618300055886
C (5)	-2.30940107675850	4.40740740740741	-7.18480334991534	10.51851851851852	-14.23021890052016
C (6)	1.00000000000000	-2.69430125621825	5.62962962962963	-9.92187129274024	15.58984910836763
C (7)		1.00000000000000	-3.7920143567800	7.00000000000000	-13.25767284805807
C (8)			1.00000000000000	-3.46410161513775	8.51851851851852
C (9)				1.00000000000000	-3.84900179459751
C (10)					1.00000000000000
	n=11	n=12	n=13	n=14	n=15
C (0)	-0.05664863918831	0.04281362620447	-0.03282202283009	0.02554291645940	-0.01991895613901
C (1)	0.47741489996416	-0.40061874199974	0.33351323347279	-0.27622596446631	0.22791919247203
C (2)	-2.01645336555843	1.84817589242163	-1.66979186788285	1.49042472299394	-1.31681813743140
C (3)	5.62695388575590	-5.63446334048794	5.52317490105692	-5.3166774494338	5.03828279717029
C (4)	-11.50378893322065	12.63667462615794	-13.47734669432089	14.01981614348744	-14.27562172334597
C (5)	18.11761418482955	-21.97937833202105	25.63667462615794	-28.92532587332406	31.74103135521054
C (6)	-22.51692449028804	30.47441954986537	-39.15410421811106	48.2030534785235	-57.25671634070853
C (7)	22.22633744855967	-34.08029737142384	48.77295127775238	-66.04388819275667	85.4476372165490
C (8)	-17.24923026467771	30.70781893004115	-49.76247176142865	74.98958492099782	-106.60227284003826
C (9)	10.18518518518519	-21.95356579140799	41.33607681755830	-70.5329790626770	111.5355687649240
C (10)	-4.23390197405726	12.00000000000000	-27.42770167705778	54.43484224956706	-97.49378990093458
C (11)	1.00000000000000	-4.61880215351701	13.96296296296296	-33.72666017043592	70.34979423868313
C (12)		1.00000000000000	-5.00370233297676	16.07407407407407	-40.91346352035126
C (13)			1.00000000000000	-5.38860251243651	18.33333333333333
C (14)				1.00000000000000	-5.77350269189626
C (15)					1.00000000000000